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Bistatic Radar Cross Sections of  
Horizontally Oriented Chaff

Peyton Z. Peebles, Jr.

March 1984

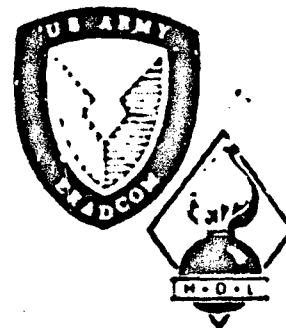
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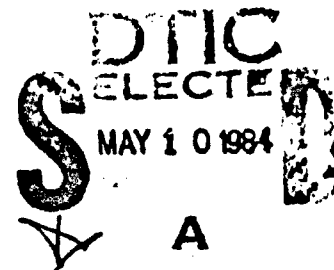
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <p>Bistatic Radar Cross sections are determined for scattering from a cloud of randomly positioned resonant dipoles (chaff). Dipoles are assumed to be horizontally oriented with axes randomly oriented in the horizontal plane. The cloud is arbitrarily located relative to an illuminating source having an arbitrary (elliptical) polarization. Cloud cross section is found for an arbitrarily located receiver that views the cloud with an antenna of arbitrary polarization. A cross section applicable to the receiver's orthogonal polarization is also found.</p>														

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## 1. INTRODUCTION

In earlier work<sup>1,2</sup> bistatic radar cross sections were determined for scattering from a cloud of randomly positioned resonant dipoles (chaff) having axes randomly and uniformly distributed in direction over a sphere. In this paper we again consider scattering from a cloud of randomly positioned dipoles, but extend the earlier work to the case where dipole axes all lie in a horizontal plane with random and uniform distribution of directions within the plane. For some practical chaff the horizontal distribution is more realistic than the spherical distribution.

The geometry applicable to a typical dipole is shown in figure 1. The axis of the dipole has its midpoint at D, the origin of coordinate system  $x', y', z'$ . Point D is in the coordinate frame  $x, y, z$  with spherical coordinates  $(r_1, \theta_1, \phi_1)$ . A transmitter at point T radiates an arbitrarily polarized wave toward D. A receiver at point R, located at  $(r_2, \theta_2, \phi_2)$  in spherical coordinates within the  $x', y', z'$  frame, receives bistatic scattering from the dipole. The receiver is presumed to have a preferred, but arbitrary, polarization that can be different than that of the transmitter. Axes of the  $x', y', z'$  frame are parallel, respectively, to those of the  $x, y, z$  frame. The axis of the dipole is assumed to lie in the  $x', y'$  plane and form an angle  $\phi_d$  from the  $x'$  axis. The angle  $\phi_d$  is assumed random with uniform distribution on  $(0, 2\pi)$ .

More generally, for fixed points T and R, scattering at R is due to many dipoles in a cloud. These dipoles are assumed to be distributed randomly and uniformly in position so that the cross sections seen at point R become the cross sections of a single dipole multiplied by N, the number of common dipoles illuminated by T and viewed by the receiver at R.<sup>1,2</sup> Other assumptions leading to this result are given in earlier work.<sup>1,2,\*</sup> Thus, only a single dipole requires analysis.

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<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

<sup>2</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, University of Florida, Electronic Communications Laboratory, prepared the report for Harry Diamond Laboratories, HDL-CR-33-107-6 (June 1983).

\* Mainly,  $r_1$  and  $r_2$  are large enough that they have approximately the same values for all dipoles of interest (those in the common volume of intersection of transmit and receive antenna patterns).

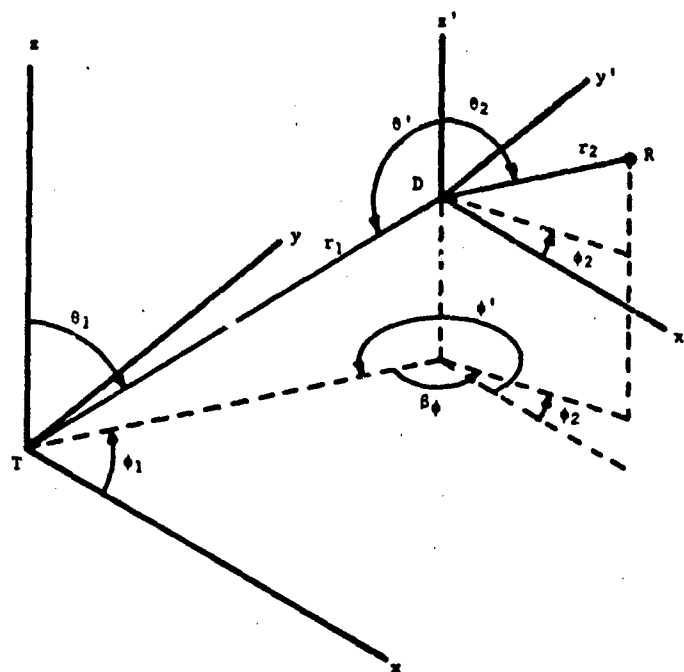


Figure 1. Geometry of bistatic scattering. A transmitter is located at point T, a receiver is at R and the scattering dipole is at point D.

## 2. ANALYSIS

Unfortunately, for the planar dipole distribution there seems to be no simple way to separate dipole scattering from transmit-receive station geometry, as was done in earlier work<sup>1</sup> using the scattering plane approach for a spherical dipole distribution. Because of this fact a direct approach to analysis is indicated. As a consequence, the resulting cross-section formulas are somewhat more cumbersome than for the spherical distribution, but can still be obtained.

### 2.1 General Equations

Consider first a very thin highly conducting dipole of total physical length  $L$ , having its wire axis pointing in the direction  $(\theta_d, \phi_d)$  in spherical coordinates. It is helpful to think of the dipole as located at point D in figure 1. Let P be an arbitrary point at  $(r, \theta, \phi)$  from the dipole in spherical coordinates. If the dipole radiates due to excitation by a terminal current

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEF Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

$I_T$ , the electric field components  $E_\theta$  and  $E_\phi$  in directions  $\theta$  and  $\phi$  at P are known.<sup>3</sup> In matrix notation they may be written as

$$\begin{bmatrix} E_\theta \\ E_\phi \end{bmatrix} = \frac{-j\eta e^{j[\omega t - (2\pi r/\lambda)]}}{2\lambda r} \begin{bmatrix} h_\theta \\ h_\phi \end{bmatrix} I_T, \quad (1)$$

where  $\eta$  is the intrinsic impedance of the medium ( $\eta = 120\pi$  for free space),  $j = \sqrt{-1}$ ,  $\omega$  is angular frequency,  $\lambda$  is wavelength,  $t$  is time, and

$$\begin{bmatrix} h_\theta \\ h_\phi \end{bmatrix} = A \begin{bmatrix} \cos \theta \sin \theta_d \cos(\phi - \phi_d) - \sin \theta \cos \theta_d \\ \sin \theta_d \sin(\phi_d - \phi) \end{bmatrix}, \quad (2)$$

$$A = \frac{(\lambda/\pi)}{\sin(\pi L/\lambda)} \cdot \frac{\cos\left[\frac{\pi L}{\lambda} \cos \psi\right] - \cos(\pi L/\lambda)}{\sin^2 \psi}, \quad (3)$$

$$\cos \psi = \cos \theta \cos \theta_d + \sin \theta \sin \theta_d \cos(\phi - \phi_d). \quad (4)$$

Here  $h_\theta$  and  $h_\phi$  are the effective lengths of the dipole evaluated in the direction  $(\theta, \phi)$ .

The current  $I_T$  that excites the fields of equation (1) is induced by fields at D that are presumed to be due to a source in a direction possibly different from that of point P (actually due to the transmitter at T in figure 1). If  $(\theta', \phi')$  is the direction of the source, the terminal current becomes

$$I_T = \frac{1}{Z_{\text{rad}}} \begin{bmatrix} h_{\theta'} & h_{\phi'} \end{bmatrix} \begin{bmatrix} E_{\theta'} \\ E_{\phi'} \end{bmatrix}, \quad (5)$$

where  $Z_{\text{rad}}$  is the dipole's radiation impedance,  $E_{\theta'}$  and  $E_{\phi'}$  are field components at the dipole in directions  $\theta'$  and  $\phi'$ , respectively, and  $h_{\theta'}$  and  $h_{\phi'}$  are equal to  $h_\theta$  and  $h_\phi$  of equation (2) evaluated for  $\theta = \theta'$ ,  $\phi = \phi'$ .

<sup>3</sup>

Cross, J. L., Response of Arrays to Stochastic Fields, Ph.D. dissertation, University of Florida (1969).



## 2.2 Special Equations

For the problem at hand,  $\theta'$  and  $\phi'$  define the location of the transmitter relative to the dipole in figure 1, while  $\theta$  and  $\phi$  define the receiver's location. Thus, we set  $\theta = \theta_2$ ,  $\phi = \phi_2$ ,  $E_\theta = E_{\theta_2}$ ,  $E_\phi = E_{\phi_2}$ ,  $\theta' = \pi - \theta_1$ ,  $\phi' = \pi + \phi_1$ ,  $E_{\theta'} = E_{\theta_1}$ , and  $E_{\phi'} = -E_{\phi_1}$  in the general equations. Here we define  $E_{\theta_1}$  and  $E_{\phi_1}$  as electric field components at D in directions  $\theta_1$  and  $\phi_1$ , respectively, due to the transmitter at T. By using the additional fact that  $\theta_d = \pi/2$  for the dipoles of interest here, we substitute equation (5) into (1) to obtain

$$\begin{bmatrix} E_{\theta_2} \\ E_{\phi_2} \end{bmatrix} = \begin{bmatrix} d_{11} & d_{12} \\ d_{21} & d_{22} \end{bmatrix} \begin{bmatrix} E_{\theta_1} \\ E_{\phi_1} \end{bmatrix} B e^{j\omega t}, \quad (6)$$

where

$$B = \frac{-j\eta e^{-j2\pi r_2/\lambda}}{2\lambda Z_{\text{rad}} r_2}, \quad (7)$$

$$d_{11} = A_1 A_0 \cos \theta_1 \cos \theta_2 \cos(\phi_1 - \phi_d) \cos(\phi_2 - \phi_d), \quad (8a)$$

$$d_{12} = -A_1 A_0 \cos \theta_2 \sin(\phi_1 - \phi_d) \cos(\phi_2 - \phi_d), \quad (8b)$$

$$d_{21} = -A_1 A_0 \cos \theta_1 \cos(\phi_1 - \phi_d) \sin(\phi_2 - \phi_d), \quad (8c)$$

$$d_{22} = A_1 A_0 \sin(\phi_1 - \phi_d) \sin(\phi_2 - \phi_d), \quad (8d)$$

and

$$A_0 = \frac{\cos\left[\frac{\pi L}{\lambda} \cos \psi_1\right] - \cos\left(\frac{\pi L}{\lambda}\right)}{\sin^2 \psi_1} \cdot \frac{\cos\left[\frac{\pi L}{\lambda} \cos \psi_2\right] - \cos\left(\frac{\pi L}{\lambda}\right)}{\sin^2 \psi_2}, \quad (9)$$

$$A_1 = (\lambda/\pi)^2 / \sin^2(\pi L/\lambda), \quad (10)$$

with

$$\cos \psi_1 = -\sin \theta_1 \cos(\phi_1 - \phi_d), \quad (11)$$

$$\cos \psi_2 = \sin \theta_2 \cos(\phi_2 - \phi_d). \quad (12)$$

### 2.3 Cross Sections

We only briefly outline the development of cross section formulas because the procedures follow those in the earlier work.<sup>1</sup> The total received electric-field vector, denoted by  $\vec{E}_2$ , can be decomposed into two orthogonally polarized components  $\vec{E}_{R1}$  and  $\vec{E}_{R2}$  that have "amplitudes"  $E_{R1}$  and  $E_{R2}$ , respectively.  $\vec{E}_R$  has the arbitrary polarization of the receiver that is determined by the receiver's field component ratio,  $Q_R$ .<sup>1</sup> The power in  $\vec{E}_{R1}$  is proportional to

$$|\vec{E}_{R1}|^2 = (1 + |Q_R|^2) |E_{R1}|^2 \quad (13)$$

Similarly, the power in the orthogonally polarized field component is proportional to

$$|\vec{E}_{R2}|^2 = (1 + |Q_R|^2) |E_{R2}|^2 \quad (14)$$

Furthermore,<sup>1</sup>

$$\begin{bmatrix} E_{R1} \\ E_{R2} \end{bmatrix} = \frac{1}{1 + |Q_R|^2} \begin{bmatrix} 1 & Q_R^* \\ -Q_R & 1 \end{bmatrix} \begin{bmatrix} E_{\theta 2} \\ E_{\phi 2} \end{bmatrix}, \quad (15)$$

where \* represents complex conjugation.

In an analogous manner, the field components  $E_{\theta 1}$  and  $E_{\phi 1}$  are related to the transmitter's field component ratio, denoted as  $Q_T$ , by<sup>1</sup>

$$\begin{bmatrix} E_{\theta 1} \\ E_{\phi 1} \end{bmatrix} = \begin{bmatrix} 1 \\ Q_T \end{bmatrix} E_T, \quad (16)$$

where  $E_T$  is the complex "amplitude" of the electric field vector, denoted by  $\vec{E}_1$ , incident on the dipole. By substituting equations (6) and (16) into (15) we have

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

$$\begin{bmatrix} E_{R1} \\ E_{R2} \end{bmatrix} = \frac{B e^{j\omega t}}{1 + |Q_R|^2} \begin{bmatrix} 1 & Q_R^* \\ -Q_R & 1 \end{bmatrix} \begin{bmatrix} d_{11} & d_{12} \\ d_{21} & d_{22} \end{bmatrix} \begin{bmatrix} 1 \\ Q_T \end{bmatrix} E_T \quad (17)$$

Next, as in the earlier work,<sup>1</sup> we define average cross sections by

$$\bar{\sigma} = 4\pi r_2^2 E[|\hat{E}_{R1}|^2] / |\hat{E}_1|^2 = \frac{4\pi r_2^2 (1 + |Q_R|^2) E[|E_{R1}|^2]}{(1 + |Q_T|^2) |E_T|^2} \quad (18)$$

$$\bar{\sigma}_x = 4\pi r_2^2 E[|\hat{E}_{R2}|^2] / |\hat{E}_1|^2 = \frac{4\pi r_2^2 (1 + |Q_R|^2) E[|E_{R2}|^2]}{(1 + |Q_T|^2) |E_T|^2} \quad (19)$$

where  $E[\cdot]$  represents the statistical expectation operation, and  $r_2$  is assumed large. The second forms of equations (15) and (16) derive from the use of equations (13) and (14), and the fact that

$$|\hat{E}_1|^2 = (1 + |Q_T|^2) |E_T|^2 \quad (20)$$

Solutions for  $\bar{\sigma}$  and  $\bar{\sigma}_x$  follow from solving equation (17) for  $E_{R1}$  and  $E_{R2}$  and substituting these quantities into equations (18) and (19). The expectations involved are each found to contain 16 terms of the form  $d_{ij} d_{mn}^*$ . Examination of these terms, using equation (8), shows that some terms are equal according to the following definitions:

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

$$\begin{aligned}
z_1 &\triangleq d_{11}d_{11}^* , \\
z_2 &\triangleq d_{11}d_{12}^* = d_{12}d_{11}^* , \\
z_3 &\triangleq d_{12}d_{12}^* , \\
z_4 &\triangleq d_{21}d_{21}^* , \\
z_5 &\triangleq d_{21}d_{22}^* = d_{22}d_{21}^* , \\
z_6 &\triangleq d_{22}d_{22}^* , \\
z_7 &\triangleq d_{11}d_{21}^* = d_{21}d_{11}^* , \\
z_8 &\triangleq d_{11}d_{22}^* = d_{12}d_{21}^* = d_{21}d_{12}^* + d_{22}d_{11}^* , \\
z_9 &\triangleq d_{12}d_{22}^* = d_{22}d_{12}^* .
\end{aligned}
\tag{21}$$

The number of distinct parameters is therefore reduced from 16 to 9 which makes the solutions of equations (18) and (19) somewhat simpler. Note, however, that nine parameters are now required to define cross sections, whereas only four were necessary when dipoles are spherically distributed as in the earlier work.<sup>1</sup>

If parameters  $\sigma_i$  are defined according to

$$\sigma_i \triangleq 4\pi r_2^2 E[|B|^2 z_i] , \quad i = 1, 2, \dots, 9 , \tag{22}$$

the solutions for the cross sections can be written as

$$\begin{aligned}
\sigma = \frac{1}{(1 + |Q_T|^2)(1 + |Q_R|^2)} &\left\{ [\sigma_1 + 2\sigma_2 \operatorname{Re}(Q_T) + \sigma_3 |Q_T|^2] \right. \\
&+ 2 \operatorname{Re}(Q_R) [\sigma_7 + 2\sigma_8 \operatorname{Re}(Q_T) + \sigma_9 |Q_T|^2] \\
&\left. + |Q_R|^2 [\sigma_4 + 2\sigma_5 \operatorname{Re}(Q_T) + \sigma_6 |Q_T|^2] \right\} .
\end{aligned}
\tag{23}$$

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

$$\bar{\sigma}_x = \frac{1}{(1 + |Q_T|^2)(1 + |Q_R|^2)} \left\{ [\sigma_4 + 2\sigma_5 \operatorname{Re}(Q_T) + \sigma_6 |Q_T|^2] \right. \\ \left. - 2 \operatorname{Re}(Q_R) [\sigma_7 + 2\sigma_8 \operatorname{Re}(Q_T) + \sigma_9 |Q_T|^2] \right. \\ \left. + |Q_R|^2 [\sigma_1 + 2\sigma_2 \operatorname{Re}(Q_T) + \sigma_3 |Q_T|^2] \right\} \quad (24)$$

Here  $\operatorname{Re}[\cdot]$  represents the real part of the bracketed quantity. Specific expressions for the parameters  $\sigma_i$  derive from equation (22) using equations (21) and (7). They are

$$\sigma_1/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \cos^2 \phi_d \cos^2(\phi_d - \beta_\phi) d\phi_d \cos^2 \theta_1 \cos^2 \theta_2, \quad (25a)$$

$$\sigma_2/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \cos \phi_d \sin \phi_d \cos^2(\phi_d - \beta_\phi) d\phi_d \cos \theta_1 \cos^2 \theta_2, \quad (25b)$$

$$\sigma_3/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \sin^2 \phi_d \cos^2(\phi_d - \beta_\phi) d\phi_d \cos^2 \theta_2, \quad (25c)$$

$$\sigma_4/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \cos^2 \phi_d \sin^2(\phi_d - \beta_\phi) d\phi_d \cos^2 \theta_1, \quad (25d)$$

$$\sigma_5/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \sin \phi_d \cos \phi_d \sin^2(\phi_d - \beta_\phi) d\phi_d \cos \theta_1, \quad (25e)$$

$$\sigma_6/\lambda^2 = A_a \int_0^{2\pi} A_0^2 \sin^2 \phi_d \sin^2(\phi_d - \beta_\phi) d\phi_d, \quad (25f)$$

$$\sigma_7/\lambda^2 = -A_a \int_0^{2\pi} A_0^2 \cos^2 \phi_d \cos(\phi_d - \beta_\phi) \sin(\phi_d - \beta_\phi) d\phi_d \cos^2 \theta_1 \cos \theta_2, \quad (25g)$$

$$\sigma_8/\lambda^2 = -A_a \int_0^{2\pi} A_0^2 \cos \phi_d \sin \phi_d \cos(\phi_d - \beta_\phi) \sin(\phi_d - \beta_\phi) d\phi_d \cos \theta_1 \cos \theta_2, \quad (25h)$$

$$\sigma_9/\lambda^2 = -A_a \int_0^{2\pi} A_0^2 \sin^2 \phi_d \cos(\phi_d - \beta_\phi) \sin(\phi_d - \beta_\phi) d\phi_d \cos \theta_2, \quad (25i)$$

where we define

$$A_a \triangleq [\eta/\sqrt{2} Z_{rad} \pi^2 \sin^2(\pi L/\lambda)]^2, \quad (26)$$

$$\beta_\phi \triangleq \pi + \phi_2 - \phi_1. \quad (27)$$

## 2.4 Coefficient Evaluation

To use equations (23) or (24) the coefficients of (25) must be evaluated. Because of the complexity of the integrands, mainly due to  $A_0$  of (9), closed solutions for the integrals were not obtained. Solutions were obtained, however, using a digital computer. Coefficients depend on the three variables  $\theta_1$ ,  $\theta_2$ , and  $\beta_\phi$ , once a particular relative dipole length is chosen ( $L/\lambda$  sets  $Z_{rad}$ , see the earlier paper<sup>1</sup>). The symmetry of (25) as a function of  $\theta_1$  or  $\theta_2$  can be analytically determined. Symmetry of (25) with  $\beta_\phi$  was determined by computer. Table 1 gives a summary of results.

TABLE 1. SYMMETRY OF COEFFICIENTS WITH VARIATIONS IN  $\theta_1$ ,  $\theta_2$ , and  $\beta_\phi$

i in $\sigma_i$	Symmetry <sup>†</sup> of $\sigma_i$ about			
	$\theta_1 = \pi/2$	$\theta_2 = \pi/2$	$\beta_\phi = 0$	$\beta_\phi = \pi/2$
1	E	E	E	E
2	O	E	O	O
3	E	E	E	E
4	E	E	E	E
5	O	E	O	O
6	E	E	E	E
7	E	O	O	O
8	O	O	E	E
9	E	O	O	O
† E = even, O = odd				

A consequence of the results shown in Table I is that parameters  $\sigma_i$  need only be evaluated for each of the three variables  $\theta_1$ ,  $\theta_2$ , and  $\beta_\phi$  over a 90-degree range; we choose the ranges  $0 \leq \theta_1 \leq \pi/2$ ,  $0 \leq \theta_2 \leq \pi/2$ , and  $0 \leq \beta_\phi \leq \pi/2$ . Tables 2, 3, and 4 give the computed results for half-wave ( $L = \lambda/2$ ), full-wave ( $L = \lambda$ ), and three halves-wave ( $L = 3\lambda/2$ ) dipoles, respectively.

Several checks were made to verify the correctness of the computed data. For example, the backscatter point for horizontal transmit and receive polar-

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

izations with  $\theta_1 = \pi/2$  and  $\theta_2 = \pi/2$  can be solved analytically with  $L = \lambda/2$ . In this case only  $\sigma_6$  is nonzero. The average backscatter cross section was found by Bloch, Hammermesh, and Phillips<sup>4</sup> to be  $\bar{\sigma} = 0.289\lambda^2$ . Solution of  $\bar{\sigma}$  as given in equation (23) gives  $\bar{\sigma} = \sigma_6 = 0.2797\lambda^2$  where an integral given by Bloch et al.<sup>4</sup> was used. The computed data give  $\bar{\sigma} = \sigma_6 = 0.2795\lambda^2$  for an error of about 0.072 percent.

### 3. CROSS SECTIONS FOR SPECIAL CASES

Cross sections, as obtained from equation (23), can be obtained for a number of special cases of transmit and receive polarizations. We shall use subscripts on  $\bar{\sigma}$  to indicate polarizations involved. The first subscript indicates the transmitter's polarization while the second applies to the wave's polarization at the receiver. We use V and H to represent linear polarizations where electric-field components are only vertical ( $\theta_1$  or  $\theta_2$  directions) and horizontal ( $\phi_1$  or  $\phi_2$  directions). Thus  $\bar{\sigma}_{VH}$  corresponds to cross section as seen by the receiver when the transmitter transmits linear polarization only in the  $\theta_1$  (or V) direction and the receiver responds only to the linear field component in the  $\phi_2$  (or H) direction.

In an analogous manner O is used to represent circular polarization (sense, left and right, will be seen to be irrelevant). Linear polarizations tilted 45 degrees from the  $\phi$  direction ( $\phi_1$  or  $\phi_2$ ) are denoted by /, while the opposite tilt for -45 degrees is denoted by subscript \.

#### 3.1 Vertical and Horizontal Polarizations

To evaluate  $\bar{\sigma}_{VV}$  the proper values of  $Q_T$  and  $Q_R$  are both zero from the earlier work.<sup>1</sup> By use of equation (23) we have

$$\bar{\sigma}_{VV} = \sigma_1. \quad (28)$$

For  $\bar{\sigma}_{HH}$  we use  $Q_T = \infty$  and  $Q_R = \infty$  to obtain

$$\bar{\sigma}_{HH} = \sigma_6. \quad (29)$$

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

<sup>4</sup> Bloch, F., M. Hammermesh, and M. Phillips, Return Cross Sections from Random Oriented Resonant Half-Wave Length Chaff, Harvard University, Radio Research Laboratory, Technical Memorandum 411-TM-127 (June 19, 1944).

For  $\bar{\sigma}_{HV}$ ,  $Q_T = \infty$ ,  $Q_R = 0$ , and

$$\bar{\sigma}_{HV} = \sigma_3 \quad (30)$$

Similarly,

$$\bar{\sigma}_{VH} = \sigma_4 \quad (31)$$

In these four simple cases only one of the parameters  $\sigma_i$  is needed to determine cross section. We note that  $\bar{\sigma}_{VH} \neq \bar{\sigma}_{HV}$  in general.

### 3.2 Circular Polarizations

For circular polarizations we have  $Q_T = \pm j$  and  $Q_R = \pm j$  from the earlier paper.<sup>1</sup> Choice of sign determines rotation sense. Since  $\text{Re}(Q_T) = 0$  and  $\text{Re}(Q_R) = 0$  while  $|Q_T|^2 = 1$  and  $|Q_R|^2 = 1$ , regardless of sense, equation (23) readily gives

$$\bar{\sigma}_{00} = (\sigma_1 + \sigma_3 + \sigma_4 + \sigma_6)/4. \quad (32)$$

Thus, the cross section seen by the receiver does not depend on the senses of either receiver or transmitter circular polarizations. This fact was also found earlier to be true for spherically distributed dipoles.<sup>1</sup>

### 3.3 Tilted Linear Polarizations

When the linear polarization is tilted 45 degrees (/notation) or -45 degrees (\notation) from the appropriate  $\phi$  direction ( $\phi_1$  or  $\phi_2$ ) the proper values of  $Q$  ( $Q_T$  or  $Q_R$ ) are 1 or -1, respectively. On substituting these values into (23) we obtain

$$\sigma_{//} = [(\sigma_1 + 2\sigma_2 + \sigma_3) + 2(\sigma_7 + 2\sigma_8 + \sigma_9) + (\sigma_4 + 2\sigma_5 + \sigma_6)]/4, \quad (33)$$

$$\sigma_{/\backslash} = [(\sigma_1 + 2\sigma_2 + \sigma_3) - 2(\sigma_7 + 2\sigma_8 + \sigma_9) + (\sigma_4 + 2\sigma_5 + \sigma_6)]/4, \quad (34)$$

$$\sigma_{\backslash\backslash} = [(\sigma_1 - 2\sigma_2 + \sigma_3) - 2(\sigma_7 - 2\sigma_8 + \sigma_9) + (\sigma_4 - 2\sigma_5 + \sigma_6)]/4, \quad (35)$$

$$\sigma_{\backslash/} = [(\sigma_1 - 2\sigma_2 + \sigma_3) + 2(\sigma_7 - 2\sigma_8 + \sigma_9) + (\sigma_4 - 2\sigma_5 + \sigma_6)]/4. \quad (36)$$

We see that these linear polarization combinations require all nine parameters  $\sigma_i$ .

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).



By solving equations (33) through (36) we may solve for  $\sigma_8$ :

$$\sigma_8 = [(\sigma_{//} - \sigma_{\backslash})/4] + [(\sigma_{\backslash\backslash} - \sigma_{\backslash})/4] \quad (37)$$

Here  $\sigma_8$  is somewhat analogous to  $\sigma_A$  in the earlier paper.<sup>1</sup>

### 3.4 Other Combinations of Linear Polarizations

By proceeding in the same manner for various combinations of vertical, horizontal, and 45-degree tilted linear polarizations we have

$$\sigma_{V//} = (\sigma_1 + 2\sigma_7 + \sigma_4)/2 \quad (38)$$

$$\sigma_{V\backslash} = (\sigma_1 - 2\sigma_7 + \sigma_4)/2 \quad (39)$$

$$\sigma_{/V} = (\sigma_1 + 2\sigma_2 + \sigma_3)/2 \quad (40)$$

$$\sigma_{\backslash V} = (\sigma_1 - 2\sigma_2 + \sigma_3)/2 \quad (41)$$

$$\sigma_{H/} = (\sigma_3 + 2\sigma_9 + \sigma_6)/2 \quad (42)$$

$$\sigma_{H\backslash} = (\sigma_3 - 2\sigma_9 + \sigma_6)/2 \quad (43)$$

$$\sigma_{/H} = (\sigma_4 + 2\sigma_5 + \sigma_6)/2 \quad (44)$$

$$\sigma_{\backslash H} = (\sigma_4 - 2\sigma_5 + \sigma_6)/2 \quad (45)$$

One of the advantages of developing equations (38) through (45) is that all remaining parameters  $\sigma_1$  can be derived as follows:

$$\sigma_2 = (\sigma_{/V} - \sigma_{\backslash V})/2 \quad (46)$$

$$\sigma_5 = (\sigma_{/H} - \sigma_{\backslash H})/2 \quad (47)$$

$$\sigma_7 = (\sigma_{V//} - \sigma_{V\backslash})/2 \quad (48)$$

$$\sigma_9 = (\sigma_{H/} - \sigma_{H\backslash})/2 \quad (49)$$

## 4. SUMMARY

An analysis has been given for bistatic radar scattering from a chaff cloud consisting of resonant dipoles randomly positioned in space in a uniform manner. Dipole axes were assumed to lie in a horizontal plane with random,

<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

uniformly distributed orientation angles within the horizontal plane. The chaff cloud is illuminated by a source having arbitrary polarization and arbitrary location relative to the cloud. The average bistatic cross section seen by a receiver of arbitrary location and arbitrary polarization was found and is given by equation (23). The cross section seen by the receiver in the orthogonal receiver polarization is given by equation (24). Both equations (23) and (24) apply to a single dipole. Cloud cross sections result from multiplication of equations (23) or (24) by  $N$ , the number of dipoles illuminated by the transmitter and viewed in common by the receiver.

Solutions of equations (23) and (24) require (1) specification of transmit and receive polarizations by defining values of  $Q_T$  and  $Q_R$  according to examples given, or from the earlier paper<sup>1</sup> in general; (2) specification of geometry parameters  $\theta_1$ ,  $\theta_2$ , and  $\beta_\phi$  (figure 1); (3) specification of resonant dipole length ( $L = \lambda/2$ ,  $\lambda$ , or  $3\lambda/2$  only); (4) determining the cross section parameters  $\sigma_1/\lambda^2$  needed from tables 2, 3, or 4 using table 1--depending on choices of  $Q_T$  and  $Q_R$  some of the  $\sigma$  may not be required; and (5) computation of equations (23) or (24). The numerical results obtained will equal  $\bar{\sigma}/\lambda^2$  or  $\bar{\sigma}_x/\lambda^2$ . Actual cross sections per dipole require  $\lambda$  be specified.

Equation (23) was used to develop cross sections in section 3 for several specific transmit/receive polarization combinations of linear, tilted linear, and circular polarizations.

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<sup>1</sup> Peebles, Peyton Z., Jr., Bistatic Radar Cross Sections of Chaff, IEEE Trans. Aerosp. Electron. Syst., AES-20, No. 2 (March 1984).

TABLE 2. PARAMETERS  $\sigma_i$ ,  $i = 1, 2, \dots, 9$ , NORMALIZED TO  $\lambda^2$   
FOR SCATTERING FROM A HALF-WAVELENGTH DIPOLE  
( $L = \lambda/2$ ). ANGLES  $\theta_1$ ,  $\theta_2$ , AND  $\beta_\phi$  SHOWN IN DEGREES.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
0	0	0	0.3226	0.0000	0.1073	0.1073	-0.0000	0.3226	-0.0000	-0.1073	0.0000
0	0	10	0.3161	0.0368	0.1140	0.1140	-0.0368	0.3161	0.0368	-0.1010	0.0368
0	0	20	0.2974	0.0691	0.1327	0.1327	-0.0691	0.2974	0.0691	-0.0824	0.0691
0	0	30	0.2688	0.0931	0.1613	0.1613	-0.0931	0.2688	0.0931	-0.0538	0.0931
0	0	40	0.2337	0.1039	0.1964	0.1964	-0.1039	0.2337	0.1039	-0.0187	0.1039
0	0	50	0.1964	0.1039	0.2337	0.2337	-0.1039	0.1964	0.1039	0.0187	0.1039
0	0	60	0.1613	0.0931	0.2688	0.2688	-0.0931	0.1613	0.0931	0.0538	0.0931
0	0	70	0.1327	0.0691	0.2974	0.2974	-0.0691	0.1327	0.0691	0.0824	0.0691
0	0	80	0.1140	0.0368	0.3161	0.3161	-0.0368	0.1140	0.0368	0.1010	0.0368
0	0	90	0.1073	0.0000	0.3226	0.3226	0.0000	0.1073	0.0000	0.1073	0.0000
0	15	0	0.2932	0.0000	0.0988	0.1038	0.0000	0.2932	0.0000	0.1022	0.0000
0	15	15	0.2873	0.0332	0.1046	0.1123	0.0368	0.3144	0.0330	0.0961	0.0350
0	15	30	0.2704	0.0623	0.1215	0.1310	0.0691	0.2957	0.0657	0.0783	0.0657
0	15	45	0.2446	0.0842	0.1474	0.1596	0.0931	0.2671	0.0885	0.0511	0.0885
0	15	60	0.2129	0.0937	0.1791	0.1947	0.1039	0.2320	0.1007	0.0178	0.1007
0	15	75	0.1791	0.0937	0.2129	0.2320	0.1039	0.1947	0.1007	0.0178	0.1007
0	15	90	0.1474	0.0842	0.2446	0.2671	0.0931	0.1596	0.0885	0.0511	0.0885
0	30	0	0.1213	0.0623	0.2704	0.2957	0.0691	0.1310	0.0657	0.0783	0.0657
0	30	15	0.1046	0.0332	0.2873	0.3144	0.0368	0.1123	0.0330	0.0961	0.0350
0	30	30	0.0988	0.0000	0.2932	0.3226	0.0000	0.1038	0.0000	0.1022	0.0000
0	30	45	0.0931	0.0332	0.2974	0.3226	0.0368	0.1038	0.0330	0.1022	0.0350
0	30	60	0.0824	0.0623	0.3161	0.3226	0.0691	0.1038	0.0657	0.1022	0.0657
0	30	75	0.0783	0.0842	0.3161	0.3226	0.0931	0.1038	0.0885	0.1022	0.0885
0	30	90	0.0783	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	0	0.0691	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	15	0.0623	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	30	0.0538	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	45	0.0479	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	60	0.0435	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	75	0.0404	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	45	90	0.0368	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	0	0.0332	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	15	0.0304	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	30	0.0270	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	45	0.0237	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	60	0.0200	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	75	0.0166	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	60	90	0.0133	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	0	0.0119	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	15	0.0092	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	30	0.0069	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	45	0.0048	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	60	0.0030	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	75	0.0016	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	75	90	0.0000	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	0	0.0000	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	15	0.0000	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	30	0.0000	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	45	0.0000	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	60	0.0000	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	75	0.0000	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
0	90	90	0.0000	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	0	0	0.3226	0.0000	0.1073	0.1073	-0.0000	0.3226	-0.0000	-0.1073	0.0000
10	0	10	0.3161	0.0368	0.1140	0.1140	-0.0368	0.3161	0.0368	-0.1010	0.0368
10	0	20	0.2974	0.0691	0.1327	0.1327	-0.0691	0.2974	0.0691	-0.0824	0.0691
10	0	30	0.2688	0.0931	0.1613	0.1613	-0.0931	0.2688	0.0931	-0.0538	0.0931
10	0	40	0.2337	0.1039	0.1964	0.1964	-0.1039	0.2337	0.1039	-0.0187	0.1039
10	0	50	0.1964	0.1039	0.2337	0.2337	-0.1039	0.1964	0.1039	0.0187	0.1039
10	0	60	0.1613	0.0931	0.2688	0.2688	-0.0931	0.1613	0.0931	0.0538	0.0931
10	0	70	0.1327	0.0691	0.2974	0.2974	-0.0691	0.1327	0.0691	0.0824	0.0691
10	0	80	0.1140	0.0368	0.3161	0.3161	-0.0368	0.1140	0.0368	0.1010	0.0368
10	0	90	0.1073	0.0000	0.3226	0.3226	0.0000	0.1073	0.0000	0.1073	0.0000
10	15	0	0.2932	0.0000	0.0988	0.1038	0.0000	0.2932	0.0000	0.1022	0.0000
10	15	15	0.2873	0.0332	0.1046	0.1123	0.0368	0.3144	0.0330	0.0961	0.0350
10	15	30	0.2704	0.0623	0.1215	0.1310	0.0691	0.2957	0.0657	0.0783	0.0657
10	15	45	0.2446	0.0842	0.1474	0.1596	0.0931	0.2671	0.0885	0.0511	0.0885
10	15	60	0.2129	0.0937	0.1791	0.1947	0.1039	0.2320	0.1007	0.0178	0.1007
10	15	75	0.1791	0.0937	0.2129	0.2320	0.1039	0.1947	0.1007	0.0178	0.1007
10	15	90	0.1474	0.0842	0.2446	0.2671	0.0931	0.1596	0.0885	0.0511	0.0885
10	30	0	0.1213	0.0623	0.2704	0.2957	0.0691	0.1310	0.0657	0.0783	0.0657
10	30	15	0.1046	0.0332	0.2873	0.3144	0.0368	0.1123	0.0330	0.0961	0.0350
10	30	30	0.0988	0.0000	0.2932	0.3226	0.0000	0.1038	0.0000	0.1022	0.0000
10	30	45	0.0931	0.0332	0.2974	0.3226	0.0368	0.1038	0.0330	0.1022	0.0350
10	30	60	0.0824	0.0623	0.3161	0.3226	0.0691	0.1038	0.0657	0.1022	0.0657
10	30	75	0.0783	0.0842	0.3161	0.3226	0.0931	0.1038	0.0885	0.1022	0.0885
10	30	90	0.0783	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	0	0.0691	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	15	0.0623	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	30	0.0538	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	45	0.0479	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	60	0.0435	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	75	0.0404	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	45	90	0.0368	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	0	0.0332	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	15	0.0304	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	30	0.0270	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	45	0.0237	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	60	0.0200	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	75	0.0166	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	60	90	0.0133	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	0	0.0119	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	15	0.0092	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	30	0.0069	0.0000	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	45	0.0048	0.0332	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	60	0.0030	0.0623	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	75	0.0016	0.0842	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	0.1007
10	75	90	0.0000	0.0937	0.3161	0.3226	0.1039	0.1038	0.1007	0.1022	

Table 2 continued, part 2 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
15	0	0	0.2932	0.0000	0.1058	0.0908	-0.0000	0.3209	-0.0000	-0.1022	0.0000
15	0	0	0.2873	0.0350	0.1123	0.1046	-0.0350	0.3144	0.0332	-0.0951	-0.0268
15	0	0	0.2704	0.0657	0.1310	0.1215	-0.0657	0.2957	0.0623	-0.0783	-0.0591
15	0	0	0.2446	0.0885	0.1596	0.1474	-0.0885	0.2671	0.0842	-0.0511	-0.0931
15	0	0	0.2129	0.1007	0.1947	0.1791	-0.1007	0.2330	0.0957	-0.0178	-0.1059
15	0	0	0.1791	0.1007	0.2320	0.2129	-0.1007	0.1947	0.0957	0.0178	-0.1059
15	0	0	0.1474	0.0885	0.2671	0.2446	-0.0885	0.1596	0.0842	0.0511	-0.0931
15	0	0	0.1215	0.0657	0.2957	0.2704	-0.0657	0.1310	0.0623	0.0783	-0.0591
15	0	0	0.1046	0.0350	0.3144	0.2973	-0.0350	0.1123	0.0332	0.0951	-0.0268
15	0	0	0.0908	-0.0000	0.3209	0.2932	-0.0000	0.1058	-0.0000	0.1022	0.0000
15	0	15	0.2665	0.0000	0.0772	0.0972	-0.0000	0.3192	-0.0000	-0.0972	0.0000
15	0	15	0.2612	0.0316	0.1031	0.1031	-0.0330	0.3127	0.0316	-0.0914	-0.0330
15	0	15	0.2459	0.0594	0.1200	0.1200	-0.0657	0.2941	0.0594	-0.0745	-0.0657
15	0	15	0.2225	0.0801	0.1458	0.1453	-0.0885	0.2655	0.0801	-0.0486	-0.0885
15	0	15	0.1939	0.0910	0.1776	0.1776	-0.1007	0.2304	0.0910	-0.0189	-0.1007
15	0	15	0.1633	0.0910	0.2113	0.2113	-0.1007	0.1900	0.0910	0.0189	-0.1007
15	0	15	0.1346	0.0801	0.2431	0.2431	-0.0885	0.1579	0.0801	0.0486	-0.0885
15	0	15	0.1113	0.0594	0.2689	0.2689	-0.0657	0.1273	0.0594	0.0745	-0.0657
15	0	15	0.0960	0.0316	0.2858	0.2858	-0.0350	0.1107	0.0316	0.0914	-0.0350
15	0	15	0.0907	-0.0000	0.2917	0.2917	-0.0000	0.1042	-0.0000	0.0972	0.0000
15	0	30	0.1994	0.0000	0.0749	0.0932	-0.0000	0.3148	-0.0000	-0.0932	0.0000
15	0	30	0.1955	0.0233	0.0792	0.0991	-0.0330	0.3053	0.0272	-0.0853	-0.0301
15	0	30	0.1843	0.0438	0.0917	0.1159	-0.0657	0.2876	0.0511	-0.0640	-0.0563
15	0	30	0.1670	0.0590	0.1108	0.1418	-0.0885	0.2610	0.0683	-0.0418	-0.0781
15	0	30	0.1459	0.0671	0.1341	0.1735	-0.1007	0.2359	0.0782	-0.0143	-0.0863
15	0	30	0.1234	0.0671	0.1590	0.2073	-0.1006	0.2073	0.0782	0.0143	-0.0863
15	0	30	0.1022	0.0590	0.1824	0.2370	-0.0885	0.1824	0.0683	0.0418	-0.0781
15	0	30	0.0850	0.0438	0.2015	0.2648	-0.0657	0.1550	0.0510	0.0640	-0.0564
15	0	30	0.0738	0.0233	0.2139	0.2817	-0.0349	0.1250	0.0272	0.0783	-0.0300
15	0	30	0.0699	-0.0000	0.2182	0.2875	-0.0000	0.0998	-0.0000	0.0733	0.0000
15	0	45	0.1205	0.0000	0.0471	0.0880	-0.0000	0.3059	-0.0000	-0.0644	0.0000
15	0	45	0.1182	0.0138	0.0497	0.0938	-0.0349	0.3024	0.0209	-0.0593	-0.0232
15	0	45	0.1115	0.0259	0.0571	0.1107	-0.0657	0.2858	0.0394	-0.0493	-0.0435
15	0	45	0.1013	0.0349	0.0683	0.1366	-0.0885	0.2532	0.0530	-0.0322	-0.0536
15	0	45	0.0888	0.0396	0.0822	0.1683	-0.1006	0.2201	0.0603	-0.0111	-0.0667
15	0	45	0.0755	0.0396	0.0968	0.2020	-0.1005	0.1828	0.0603	0.0112	-0.0666
15	0	45	0.0630	0.0348	0.1107	0.2336	-0.0884	0.1478	0.0530	0.0322	-0.0536
15	0	45	0.0529	0.0259	0.1219	0.2594	-0.0656	0.1193	0.0393	0.0493	-0.0435
15	0	45	0.0462	0.0138	0.1292	0.2763	-0.0349	0.1007	0.0209	0.0603	-0.0231
15	0	45	0.0439	-0.0000	0.1318	0.2821	-0.0000	0.0942	-0.0000	0.0543	0.0000
15	0	60	0.0345	0.0000	0.0223	0.0831	-0.0000	0.3033	-0.0000	-0.0430	0.0000
15	0	60	0.0335	0.0061	0.0234	0.0889	-0.0349	0.2968	0.0140	-0.0404	-0.0155
15	0	60	0.0306	0.0114	0.0266	0.1058	-0.0656	0.2781	0.0263	-0.0329	-0.0291
15	0	60	0.0461	0.0154	0.0316	0.1316	-0.0883	0.2496	0.0354	-0.0215	-0.0392
15	0	60	0.0405	0.0175	0.0377	0.1633	-0.1004	0.2146	0.0402	-0.0074	-0.0445
15	0	60	0.0347	0.0175	0.0442	0.1969	-0.1004	0.1773	0.0402	0.0075	-0.0445
15	0	60	0.0292	0.0154	0.0503	0.2285	-0.0832	0.1424	0.0353	0.0215	-0.0571
15	0	60	0.0247	0.0114	0.0553	0.2543	-0.0655	0.1139	0.0262	0.0329	-0.0290
15	0	60	0.0217	0.0061	0.0585	0.2711	-0.0348	0.0953	0.0140	0.0403	-0.0154
15	0	60	0.0207	-0.0000	0.0596	0.2769	-0.0000	0.0889	-0.0000	0.0429	0.0000
15	0	75	0.0136	0.0000	0.0057	0.0796	-0.0000	0.2993	-0.0000	-0.0213	0.0000
15	0	75	0.0133	0.0015	0.0060	0.0855	-0.0349	0.2928	0.0069	-0.0201	-0.0077
15	0	75	0.0126	0.0028	0.0068	0.1024	-0.0655	0.2741	0.0130	-0.0163	-0.0144
15	0	75	0.0115	0.0038	0.0080	0.1281	-0.0882	0.2456	0.0176	-0.0107	-0.0194
15	0	75	0.0102	0.0043	0.0095	0.1598	-0.1003	0.2107	0.0200	-0.0037	-0.0221
15	0	75	0.0087	0.0043	0.0111	0.1934	-0.1002	0.1735	0.0200	0.0037	-0.0221
15	0	75	0.0074	0.0038	0.0126	0.2249	-0.0881	0.1386	0.0175	0.0107	-0.0194
15	0	75	0.0063	0.0028	0.0133	0.2506	-0.0653	0.1102	0.0120	0.0163	-0.0144
15	0	75	0.0054	0.0015	0.0146	0.2674	-0.0348	0.0917	0.0059	0.0200	-0.0077
15	0	75	0.0053	-0.0000	0.0148	0.2732	-0.0000	0.0852	-0.0000	0.0213	0.0000
15	0	90	0.0000	0.0000	0.0000	0.0784	-0.0000	0.2978	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.0843	-0.0348	0.2913	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.1011	-0.0655	0.2727	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.1269	-0.0882	0.2442	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.1585	-0.1002	0.2093	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.1921	-0.1001	0.1721	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.2236	-0.0850	0.1373	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.2493	-0.0633	0.1009	-0.0000	0.0000	0.0000
15	0	90	0.0000	0.0000	0.0000	0.2660	-0.0347	0.0703	-0.0000	0.0000	0.0000
15	0	90	0.0000	-0.0000	0.0000	0.2718	0.0000	0.0539	-0.0000	0.0000	0.0000

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$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
30	0	0	0.2174	0.0000	0.1014	0.0741	-0.0000	0.3164	-0.0000	-0.0878	0.0000
30	0	0	0.2151	0.0300	0.1079	0.0804	-0.0300	0.3099	-0.0243	-0.0823	0.0368
30	0	0	0.2026	0.0365	0.1266	0.0928	-0.0365	0.2912	-0.0461	-0.0673	0.0671
30	0	0	0.1835	0.0761	0.1552	0.1119	-0.0761	0.2626	-0.0621	-0.0439	0.0931
30	0	0	0.1602	0.0865	0.1702	0.1353	-0.0865	0.2276	-0.0706	-0.0153	0.1058
30	0	0	0.1353	0.0865	0.2276	0.1602	-0.0865	0.1902	-0.0706	0.0153	0.1058
30	0	0	0.1119	0.0761	0.2626	0.1835	-0.0761	0.1552	-0.0621	0.0439	0.0931
30	0	0	0.0923	0.0565	0.2712	0.2026	-0.0565	0.1266	-0.0461	0.0673	0.0671
30	0	0	0.0804	0.0300	0.3099	0.2151	-0.0300	0.1079	-0.0243	0.0823	0.0368
30	0	0	0.0761	0.0000	0.3164	0.2194	-0.0000	0.1014	-0.0000	0.0878	0.0000
30	0	0	0.1974	0.0000	0.0932	0.0749	-0.0000	0.3148	-0.0000	0.0835	0.0000
30	1	0	0.1955	0.0272	0.0991	0.0792	-0.0301	0.3083	-0.0233	0.0785	0.0350
30	1	0	0.1843	0.0511	0.1159	0.0917	-0.0565	0.2976	-0.0438	0.0640	0.0637
30	1	0	0.1670	0.0688	0.1416	0.1108	-0.0761	0.2510	-0.0590	0.0418	0.0885
30	1	0	0.1459	0.0782	0.1735	0.1341	-0.0865	0.2239	-0.0671	0.0145	0.1006
30	1	0	0.1234	0.0782	0.2073	0.1590	-0.0865	0.1886	-0.0671	0.0145	0.1006
30	1	0	0.1022	0.0688	0.2390	0.1824	-0.0761	0.1535	-0.0590	0.0418	0.0885
30	1	0	0.0850	0.0510	0.2548	0.2013	-0.0564	0.1230	-0.0438	0.0640	0.0637
30	1	0	0.0738	0.0272	0.2817	0.2193	-0.0300	0.1063	-0.0233	0.0785	0.0350
30	1	0	0.0699	0.0000	0.2875	0.2182	-0.0000	0.0988	-0.0000	0.0835	0.0000
30	1	0	0.1493	0.0000	0.0718	0.0718	-0.0000	0.3103	-0.0000	0.0718	0.0000
30	1	0	0.1464	0.0201	0.0762	0.0762	-0.0301	0.3001	-0.0201	0.0673	0.0301
30	1	0	0.1381	0.0377	0.0886	0.0886	-0.0565	0.2933	-0.0377	0.0565	0.0565
30	1	0	0.1253	0.0507	0.1077	0.1077	-0.0761	0.2836	-0.0507	0.0350	0.0761
30	1	0	0.0977	0.0577	0.1211	0.1311	-0.0865	0.2682	-0.0577	0.0145	0.0865
30	1	0	0.0731	0.0576	0.1391	0.1560	-0.0865	0.2496	-0.0576	0.0145	0.0865
30	1	0	0.0776	0.0506	0.1594	0.1794	-0.0865	0.2300	-0.0506	0.0145	0.0865
30	1	0	0.0449	0.0376	0.1984	0.2198	-0.0865	0.2077	-0.0376	0.0145	0.0865
30	1	0	0.0566	0.0200	0.2308	0.2308	-0.0300	0.3000	-0.0200	0.0640	0.0300
30	1	0	0.0538	0.0000	0.2351	0.2351	-0.0000	0.2956	-0.0000	0.0673	0.0000
30	1	0	0.0902	0.0000	0.0452	0.0678	-0.0000	0.3048	-0.0000	0.0554	0.0000
30	1	0	0.0885	0.0119	0.0478	0.0722	-0.0301	0.2983	-0.0155	0.0320	0.0320
30	1	0	0.0836	0.0223	0.0555	0.0847	-0.0565	0.2745	-0.0391	0.0124	0.0426
30	1	0	0.0760	0.0300	0.0665	0.1038	-0.0761	0.2504	-0.0391	0.0076	0.0587
30	1	0	0.0648	0.0341	0.0803	0.1272	-0.0865	0.2196	-0.0495	0.0067	0.0667
30	1	0	0.0700	0.0340	0.0850	0.1571	-0.0865	0.1785	-0.0444	0.0077	0.0666
30	1	0	0.0678	0.0299	0.1088	0.1753	-0.0758	0.1455	-0.0390	0.0077	0.0585
30	1	0	0.0404	0.0222	0.1200	0.1943	-0.0562	0.1151	-0.0289	0.0023	0.0454
30	1	0	0.0335	0.0118	0.1273	0.2067	-0.0397	0.0966	-0.0154	0.0019	0.0331
30	1	0	0.0338	0.0000	0.1298	0.2109	-0.0000	0.0901	-0.0000	0.0000	0.0000
30	1	0	0.0409	0.0000	0.0214	0.0641	-0.0000	0.2993	-0.0000	0.0000	0.0000
30	1	0	0.0401	0.0053	0.0223	0.0684	-0.0301	0.2901	-0.0103	0.0000	0.0000
30	1	0	0.0379	0.0099	0.0258	0.0810	-0.0565	0.2740	-0.0194	0.0000	0.0000
30	1	0	0.0346	0.0133	0.0308	0.1001	-0.0760	0.2494	-0.0267	0.0000	0.0000
30	1	0	0.0305	0.0131	0.0369	0.1235	-0.0865	0.2193	-0.0397	0.0000	0.0000
30	1	0	0.0263	0.0150	0.0474	0.1483	-0.0865	0.1882	-0.0526	0.0000	0.0000
30	1	0	0.0231	0.0133	0.0493	0.1718	-0.0757	0.1632	-0.0667	0.0000	0.0000
30	1	0	0.0188	0.0098	0.0544	0.1963	-0.0562	0.1397	-0.0866	0.0000	0.0000
30	1	0	0.0167	0.0052	0.0576	0.2037	-0.0397	0.1194	-0.1033	0.0000	0.0000
30	1	0	0.0159	0.0000	0.0589	0.2070	-0.0000	0.0980	-0.0000	0.0000	0.0000
30	1	0	0.0102	0.0000	0.0590	0.0615	-0.0000	0.0850	-0.0000	0.0000	0.0000
30	1	0	0.0100	0.0013	0.0598	0.0539	-0.0000	0.0700	-0.0000	0.0000	0.0000
30	1	0	0.0095	0.0024	0.0566	0.0378	-0.0000	0.2701	-0.0097	0.0000	0.0000
30	1	0	0.0076	0.0032	0.0532	0.0273	-0.0000	0.2413	-0.0130	0.0000	0.0000
30	1	0	0.0066	0.0037	0.0497	0.0163	-0.0000	0.2064	-0.0147	0.0000	0.0000
30	1	0	0.0056	0.0022	0.0457	0.0088	-0.0000	0.1673	-0.0129	0.0000	0.0000
30	1	0	0.0048	0.0014	0.0424	0.0076	-0.0000	0.1342	-0.0096	0.0000	0.0000
30	1	0	0.0041	0.0000	0.0390	0.0041	-0.0000	0.0878	-0.0031	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0813	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.2940	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.2873	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.2688	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.2501	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.2031	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.1679	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.1332	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.1050	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0846	-0.0000	0.0000	0.0000
30	1	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0802	-0.0000	0.0000	0.0000

Table 2 continued, part 4 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
45	0	0	0.1325	0.0000	0.0957	0.0479	-0.0000	0.3105	-0.0000	-0.0677	0.0000
45	0	0	0.1300	0.0331	0.1022	0.0504	-0.0231	0.3040	0.0145	-0.0436	0.0367
45	0	0	0.1226	0.0435	0.1208	0.0578	-0.0435	0.2853	0.0272	-0.0318	0.0690
45	0	0	0.1113	0.0586	0.1494	0.0690	-0.0586	0.2568	0.0367	-0.0338	0.0930
45	0	0	0.0975	0.0667	0.1844	0.0828	-0.0667	0.2217	0.0417	-0.0118	0.1057
45	0	0	0.0828	0.0667	0.2217	0.0975	-0.0667	0.1844	0.0417	-0.0118	0.1057
45	0	0	0.0690	0.0586	0.2568	0.1113	-0.0586	0.1494	0.0367	-0.0338	0.0930
45	0	0	0.0578	0.0435	0.2853	0.1226	-0.0435	0.1208	0.0272	-0.0318	0.0690
45	0	0	0.0504	0.0331	0.3040	0.1300	-0.0231	0.1022	0.0145	-0.0436	0.0367
45	0	0	0.0479	0.0000	0.3105	0.1325	0.0000	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.1205	0.0000	0.0880	0.0471	-0.0000	0.3089	-0.0000	-0.0644	0.0000
45	0	0	0.1182	0.0209	0.0938	0.0497	-0.0232	0.3024	0.0138	-0.0603	0.0349
45	0	0	0.1115	0.0394	0.1107	0.0571	-0.0435	0.2838	0.0259	-0.0493	0.0657
45	0	0	0.1013	0.0530	0.1366	0.0683	-0.0586	0.2552	0.0349	-0.0322	0.0885
45	0	0	0.0888	0.0603	0.1683	0.0822	-0.0667	0.2201	0.0394	-0.0111	0.1006
45	0	0	0.0755	0.0603	0.2020	0.0968	-0.0667	0.1828	0.0394	-0.0111	0.1006
45	0	0	0.0630	0.0530	0.2336	0.1107	-0.0586	0.1478	0.0349	-0.0322	0.0885
45	0	0	0.0529	0.0393	0.2594	0.1214	-0.0435	0.1193	0.0259	-0.0493	0.0657
45	0	0	0.0466	0.0209	0.2763	0.1292	-0.0231	0.1007	0.0138	-0.0603	0.0349
45	0	0	0.0435	0.0000	0.2821	0.1318	0.0000	0.0942	-0.0000	-0.0644	0.0000
45	0	0	0.0400	0.0000	0.2878	0.1325	0.0000	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0372	0.0155	0.0722	0.0478	-0.0232	0.3089	-0.0000	-0.0644	0.0000
45	0	0	0.0344	0.0291	0.0847	0.0532	-0.0435	0.2838	0.0259	-0.0493	0.0657
45	0	0	0.0317	0.0391	0.1078	0.0603	-0.0586	0.2552	0.0349	-0.0322	0.0885
45	0	0	0.0290	0.0444	0.1321	0.0683	-0.0667	0.2201	0.0394	-0.0111	0.1006
45	0	0	0.0263	0.0497	0.1573	0.0755	-0.0586	0.1828	0.0349	-0.0322	0.0885
45	0	0	0.0236	0.0550	0.1825	0.0822	-0.0667	0.1478	0.0349	-0.0322	0.0885
45	0	0	0.0209	0.0603	0.2077	0.0888	-0.0667	0.1193	0.0259	-0.0493	0.0657
45	0	0	0.0182	0.0656	0.2329	0.0957	-0.0667	0.1007	0.0138	-0.0603	0.0349
45	0	0	0.0155	0.0709	0.2581	0.1022	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0128	0.0762	0.2833	0.1088	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0101	0.0815	0.3085	0.1153	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0074	0.0868	0.3337	0.1218	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0047	0.0921	0.3589	0.1283	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0020	0.0974	0.3841	0.1348	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1027	0.4093	0.1413	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1076	0.4345	0.1478	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1125	0.4597	0.1543	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1174	0.4849	0.1608	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1223	0.5101	0.1673	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1272	0.5353	0.1738	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1321	0.5605	0.1803	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1370	0.5857	0.1868	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1419	0.6109	0.1933	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1468	0.6361	0.1998	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1517	0.6613	0.2063	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1566	0.6865	0.2128	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1615	0.7117	0.2193	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1664	0.7369	0.2258	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1713	0.7621	0.2323	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1762	0.7873	0.2388	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1811	0.8125	0.2453	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1860	0.8377	0.2518	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1909	0.8629	0.2583	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.1958	0.8881	0.2648	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2007	0.9133	0.2713	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2056	0.9385	0.2778	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2105	0.9637	0.2843	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2154	0.9889	0.2908	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2203	1.0141	0.2973	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2252	1.0393	0.3038	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2301	1.0645	0.3103	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2350	1.0897	0.3168	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2399	1.1149	0.3233	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2448	1.1401	0.3298	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2497	1.1653	0.3363	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2546	1.1905	0.3428	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2595	1.2157	0.3493	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2644	1.2409	0.3558	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2693	1.2661	0.3623	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2742	1.2913	0.3688	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2791	1.3165	0.3753	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2840	1.3417	0.3818	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2889	1.3669	0.3883	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2938	1.3921	0.3948	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.2987	1.4173	0.4013	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3036	1.4425	0.4078	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3085	1.4677	0.4143	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3134	1.4929	0.4208	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3183	1.5181	0.4273	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3232	1.5433	0.4338	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3281	1.5685	0.4403	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3330	1.5937	0.4468	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3379	1.6189	0.4533	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3428	1.6441	0.4598	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3477	1.6693	0.4663	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3526	1.6945	0.4728	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3575	1.7197	0.4793	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3624	1.7449	0.4858	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3673	1.7701	0.4923	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3722	1.7953	0.4988	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3771	1.8205	0.5053	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3820	1.8457	0.5118	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3869	1.8709	0.5183	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3918	1.8961	0.5248	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.3967	1.9213	0.5313	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.4016	1.9465	0.5378	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.4065	1.9717	0.5443	-0.0667	0.0957	-0.0000	-0.0677	0.0000
45	0	0	0.0000	0.4114	1.9969	0.5508					

Table 2 continued, part 5 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
60	0	0	0.0000	0.0000	0.0704	0.0076	-0.0000	0.3047	-0.0000	-0.0452	0.0000
60	0	0	0.0000	0.0153	0.0863	0.0237	-0.0153	0.2983	0.0064	-0.0425	-0.0367
60	0	0	0.0000	0.0300	0.1154	0.0270	-0.0290	0.2797	0.0120	-0.0346	-0.0689
60	0	0	0.0000	0.0391	0.1439	0.0319	-0.0391	0.2511	0.0162	-0.0226	-0.0928
60	0	0	0.0000	0.0445	0.1709	0.0330	-0.0445	0.2162	0.0184	-0.0078	-0.1056
60	0	0	0.0000	0.0445	0.2162	0.0330	-0.0445	0.1709	0.0184	0.0078	-0.1056
60	0	0	0.0000	0.0391	0.2511	0.0306	-0.0391	0.1439	0.0162	0.0226	-0.0928
60	0	0	0.0000	0.0270	0.2797	0.0237	-0.0290	0.1154	0.0120	0.0346	-0.0689
60	0	0	0.0000	0.0153	0.2983	0.0076	-0.0153	0.0768	0.0064	0.0425	-0.0367
60	0	0	0.0000	0.0000	0.3047	0.0000	0.0000	0.0000	0.0000	0.0452	0.0000
60	0	15	0.0000	0.0000	0.0331	0.0223	-0.0000	0.3033	-0.0000	-0.0430	0.0000
60	0	15	0.0000	0.0140	0.0837	0.0234	-0.0153	0.2768	0.0061	-0.0404	-0.0349
60	0	15	0.0000	0.0266	0.1038	0.0266	-0.0291	0.2791	0.0114	-0.0329	-0.0456
60	0	15	0.0000	0.0334	0.1316	0.0316	-0.0392	0.2496	0.0154	-0.0215	-0.0883
60	0	15	0.0000	0.0402	0.1633	0.0377	-0.0445	0.2146	0.0175	-0.0074	-0.1004
60	0	15	0.0000	0.0402	0.1949	0.0442	-0.0445	0.1773	0.0175	0.0075	-0.1004
60	0	15	0.0000	0.0353	0.2265	0.0503	-0.0391	0.1424	0.0154	0.0215	-0.0882
60	0	15	0.0000	0.0262	0.2543	0.0533	-0.0290	0.1139	0.0114	0.0329	-0.0655
60	0	15	0.0000	0.0140	0.2711	0.0533	-0.0154	0.0753	0.0061	0.0403	-0.0348
60	0	15	0.0000	0.0000	0.2769	0.0596	0.0000	0.0789	-0.0000	0.0429	0.0000
60	0	30	0.0000	0.0000	0.0541	0.0214	-0.0000	0.2993	-0.0000	-0.0370	0.0000
60	0	30	0.0000	0.0103	0.0804	0.0225	-0.0153	0.2928	0.0053	-0.0348	-0.0301
60	0	30	0.0000	0.0194	0.0810	0.0238	-0.0291	0.2740	0.0099	-0.0283	-0.0565
60	0	30	0.0000	0.0261	0.1001	0.0268	-0.0392	0.2404	0.0133	-0.0184	-0.0760
60	0	30	0.0000	0.0297	0.1235	0.0349	-0.0445	0.2103	0.0151	-0.0063	-0.0863
60	0	30	0.0000	0.0296	0.1483	0.0434	-0.0444	0.1731	0.0150	0.0085	-0.0862
60	0	30	0.0000	0.0260	0.1715	0.0495	-0.0390	0.1332	0.0132	0.0185	-0.0757
60	0	30	0.0000	0.0193	0.1904	0.0544	-0.0299	0.1099	0.0098	0.0283	-0.0561
60	0	30	0.0000	0.0162	0.2027	0.0576	-0.0154	0.0714	0.0052	0.0346	-0.0298
60	0	30	0.0000	0.0000	0.2070	0.0537	0.0000	0.0750	-0.0000	0.0368	0.0000
60	0	45	0.0000	0.0000	0.0404	0.0202	-0.0000	0.2941	-0.0000	-0.0284	0.0000
60	0	45	0.0000	0.0051	0.0430	0.0214	-0.0156	0.2875	0.0041	-0.0266	-0.0233
60	0	45	0.0000	0.0115	0.0505	0.0247	-0.0292	0.2686	0.0076	-0.0218	-0.0437
60	0	45	0.0000	0.0155	0.0619	0.0297	-0.0393	0.2398	0.0103	-0.0141	-0.0587
60	0	45	0.0000	0.0175	0.0757	0.0338	-0.0445	0.2047	0.0116	-0.0048	-0.0666
60	0	45	0.0000	0.0175	0.0904	0.0423	-0.0444	0.1675	0.0116	0.0051	-0.0663
60	0	45	0.0000	0.0153	0.1041	0.0484	-0.0387	0.1328	0.0101	0.0143	-0.0582
60	0	45	0.0000	0.0113	0.1151	0.0533	-0.0288	0.1047	0.0075	0.0218	-0.0431
60	0	45	0.0000	0.0050	0.1273	0.0564	-0.0153	0.0864	0.0040	0.0266	-0.0229
60	0	45	0.0000	0.0000	0.1248	0.0575	0.0000	0.0800	-0.0000	0.0283	0.0000
60	0	60	0.0000	0.0000	0.0191	0.0191	-0.0000	0.2890	-0.0000	-0.0191	0.0000
60	0	60	0.0000	0.0037	0.0303	0.0203	-0.0156	0.2824	0.0027	-0.0180	-0.0156
60	0	60	0.0000	0.0051	0.0336	0.0236	-0.0293	0.2635	0.0051	-0.0146	-0.0293
60	0	60	0.0000	0.0089	0.0387	0.0287	-0.0393	0.2345	0.0089	-0.0099	-0.0393
60	0	60	0.0000	0.0078	0.0348	0.0348	-0.0445	0.1994	0.0078	-0.0032	-0.0445
60	0	60	0.0000	0.0077	0.0413	0.0413	-0.0442	0.1623	0.0077	0.0034	-0.0442
60	0	60	0.0000	0.0067	0.0473	0.0473	-0.0387	0.1277	0.0057	0.0096	-0.0387
60	0	60	0.0000	0.0050	0.0522	0.0522	-0.0286	0.0997	0.0050	0.0145	-0.0286
60	0	60	0.0000	0.0036	0.0553	0.0553	-0.0152	0.0816	0.0026	0.0177	-0.0152
60	0	60	0.0000	0.0000	0.0544	0.0544	0.0000	0.0753	-0.0000	0.0188	0.0000
60	0	75	0.0000	0.0000	0.0049	0.0184	-0.0000	0.2855	-0.0000	-0.0095	0.0000
60	0	75	0.0000	0.0007	0.0052	0.0196	-0.0156	0.2788	0.0014	-0.0089	-0.0078
60	0	75	0.0000	0.0013	0.0060	0.0229	-0.0293	0.2598	0.0025	-0.0072	-0.0146
60	0	75	0.0000	0.0017	0.0073	0.0260	-0.0393	0.2308	0.0034	-0.0047	-0.0195
60	0	75	0.0000	0.0019	0.0084	0.0341	-0.0444	0.1956	0.0039	-0.0015	-0.0221
60	0	75	0.0000	0.0019	0.0104	0.0406	-0.0441	0.1586	0.0038	0.0017	-0.0219
60	0	75	0.0000	0.0016	0.0118	0.0466	-0.0386	0.1241	0.0033	0.0048	-0.0192
60	0	75	0.0000	0.0012	0.0130	0.0514	-0.0295	0.0963	0.0025	0.0072	-0.0142
60	0	75	0.0000	0.0006	0.0131	0.0545	-0.0151	0.0783	0.0013	0.0088	-0.0075
60	0	75	0.0000	0.0000	0.0140	0.0556	0.0000	0.0721	-0.0000	0.0093	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0131	-0.0000	0.2842	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0193	-0.0156	0.2775	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0226	-0.0293	0.2585	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0277	-0.0393	0.2295	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0339	-0.0444	0.1943	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0403	-0.0441	0.1572	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0463	-0.0395	0.1229	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0511	-0.0285	0.0951	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0542	-0.0151	0.0771	-0.0000	0.0000	0.0000
60	0	90	0.0000	0.0000	0.0000	0.0553	0.0000	0.0709	0.0000	0.0000	0.0000

Table 2 continued, part 6 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$	
75	0	0	0	0.0149	0.0000	0.0866	0.0058	-0.0000	0.3007	-0.0000	-0.0224	0.0000
75	0	0	0	0.0147	0.0077	0.0731	0.0061	-0.0077	0.2942	-0.0016	-0.0211	-0.0366
75	0	0	0	0.0139	0.0144	0.1117	0.0069	-0.0144	0.2756	0.0029	-0.0172	-0.0688
75	0	0	0	0.0126	0.0194	0.1401	0.0081	-0.0194	0.2472	0.0040	-0.0112	-0.0927
75	0	0	0	0.0112	0.0221	0.1751	0.0096	-0.0221	0.2122	0.0043	-0.0039	-0.1034
75	0	0	0	0.0096	0.0221	0.2122	0.0112	-0.0221	0.1751	0.0043	0.0039	-0.1034
75	0	0	0	0.0081	0.0194	0.2472	0.0126	-0.0194	0.1401	0.0040	0.0112	-0.0927
75	0	0	0	0.0069	0.0144	0.2756	0.0139	-0.0144	0.1117	0.0029	0.0172	-0.0688
75	0	0	0	0.0061	0.0077	0.2942	0.0147	-0.0077	0.0931	0.0016	0.0211	-0.0366
75	0	0	0	0.0058	-0.0000	0.3007	0.0157	0.0000	0.0866	-0.0000	0.0224	0.0000
75	0	0	0	0.0136	0.0000	0.0796	0.0057	-0.0000	0.2993	-0.0000	-0.0213	0.0000
75	0	0	0	0.0133	0.0069	0.0853	0.0060	-0.0077	0.2928	0.0013	-0.0201	0.0349
75	0	0	0	0.0126	0.0130	0.1024	0.0069	-0.0144	0.2741	0.0028	-0.0163	-0.0653
75	0	0	0	0.0115	0.0176	0.1281	0.0093	-0.0194	0.2456	0.0038	-0.0107	-0.0882
75	0	0	0	0.0102	0.0200	0.1598	0.0111	-0.0221	0.2107	0.0043	-0.0037	-0.1003
75	0	0	0	0.0087	0.0200	0.1934	0.0111	-0.0221	0.1735	0.0043	0.0037	-0.1003
75	0	0	0	0.0074	0.0175	0.2249	0.0126	-0.0194	0.1386	0.0038	0.0107	-0.0882
75	0	0	0	0.0063	0.0130	0.2506	0.0138	-0.0144	0.1102	0.0028	0.0163	-0.0653
75	0	0	0	0.0056	0.0069	0.2674	0.0146	-0.0077	0.0917	0.0013	0.0200	-0.0348
75	0	0	0	0.0053	-0.0000	0.2732	0.0148	0.0000	0.0852	-0.0000	0.0213	0.0000
75	0	0	0	0.0102	0.0000	0.0613	0.0053	-0.0000	0.2954	-0.0000	-0.0184	0.0000
75	0	0	0	0.0100	0.0031	0.0659	0.0058	-0.0077	0.2889	0.0013	-0.0173	0.0301
75	0	0	0	0.0093	0.0097	0.0787	0.0066	-0.0145	0.2701	0.0024	-0.0140	-0.0363
75	0	0	0	0.0086	0.0130	0.0973	0.0078	-0.0195	0.2415	0.0033	-0.0091	-0.0759
75	0	0	0	0.0076	0.0147	0.1209	0.0093	-0.0221	0.2064	0.0037	-0.0031	-0.0862
75	0	0	0	0.0066	0.0147	0.1456	0.0109	-0.0221	0.1693	0.0037	0.0033	-0.0860
75	0	0	0	0.0056	0.0129	0.1688	0.0124	-0.0194	0.1347	0.0032	0.0092	-0.0753
75	0	0	0	0.0048	0.0096	0.1876	0.0136	-0.0143	0.1062	0.0024	0.0140	-0.0539
75	0	0	0	0.0043	0.0031	0.1999	0.0143	-0.0076	0.0878	0.0013	0.0172	-0.0297
75	0	0	0	0.0041	-0.0000	0.2041	0.0146	0.0000	0.0813	-0.0000	0.0183	0.0000
75	0	0	0	0.0042	0.0000	0.0388	0.0052	-0.0000	0.2904	-0.0000	-0.0142	0.0000
75	0	0	0	0.0060	0.0031	0.0414	0.0053	-0.0077	0.2838	0.0010	-0.0133	0.0233
75	0	0	0	0.0057	0.0057	0.0489	0.0063	-0.0145	0.2649	0.0019	-0.0108	-0.0437
75	0	0	0	0.0052	0.0077	0.0603	0.0075	-0.0195	0.2360	0.0023	-0.0070	-0.0587
75	0	0	0	0.0046	0.0077	0.0742	0.0090	-0.0221	0.2009	0.0028	-0.0024	-0.0663
75	0	0	0	0.0040	0.0087	0.0888	0.0106	-0.0220	0.1638	0.0028	0.0023	-0.0662
75	0	0	0	0.0034	0.0076	0.1024	0.0121	-0.0193	0.1292	0.0023	0.0071	-0.0580
75	0	0	0	0.0030	0.0056	0.1134	0.0133	-0.0143	0.1011	0.0018	0.0108	-0.0429
75	0	0	0	0.0027	0.0030	0.1206	0.0140	-0.0076	0.0829	0.0010	0.0132	-0.0228
75	0	0	0	0.0026	-0.0000	0.1231	0.0143	0.0000	0.0766	-0.0000	0.0140	0.0000
75	0	0	0	0.0028	0.0000	0.0184	0.0049	-0.0000	0.2853	-0.0000	-0.0093	0.0000
75	0	0	0	0.0027	0.0014	0.0196	0.0052	-0.0078	0.2788	0.0007	-0.0089	0.0136
75	0	0	0	0.0026	0.0023	0.0229	0.0060	-0.0146	0.2598	0.0013	-0.0072	-0.0293
75	0	0	0	0.0024	0.0034	0.0280	0.0073	-0.0195	0.2308	0.0017	-0.0047	-0.0393
75	0	0	0	0.0021	0.0039	0.0341	0.0088	-0.0221	0.1956	0.0019	-0.0015	-0.0444
75	0	0	0	0.0018	0.0038	0.0406	0.0104	-0.0219	0.1586	0.0019	0.0017	-0.0441
75	0	0	0	0.0016	0.0033	0.0466	0.0118	-0.0192	0.1241	0.0016	0.0048	-0.0386
75	0	0	0	0.0014	0.0023	0.0514	0.0130	-0.0142	0.0963	0.0012	0.0072	-0.0283
75	0	0	0	0.0013	0.0013	0.0543	0.0138	-0.0075	0.0783	0.0004	0.0088	-0.0151
75	0	0	0	0.0012	-0.0000	0.0556	0.0140	0.0000	0.0721	-0.0000	0.0093	0.0000
75	0	0	0	0.0007	0.0000	0.0477	0.0047	-0.0000	0.2850	-0.0000	-0.0047	0.0000
75	0	0	0	0.0007	0.0003	0.0050	0.0030	-0.0078	0.2753	0.0003	-0.0044	0.0078
75	0	0	0	0.0006	0.0006	0.0053	0.0038	-0.0146	0.2562	0.0006	-0.0036	-0.0146
75	0	0	0	0.0006	0.0008	0.0057	0.0051	-0.0195	0.2271	0.0008	-0.0023	-0.0193
75	0	0	0	0.0005	0.0009	0.0064	0.0065	-0.0221	0.1979	0.0009	-0.0008	-0.0221
75	0	0	0	0.0005	0.0009	0.0102	0.0085	-0.0219	0.1549	0.0009	0.0009	-0.0219
75	0	0	0	0.0004	0.0008	0.0116	0.0102	-0.0191	0.1206	0.0008	0.0024	-0.0191
75	0	0	0	0.0004	0.0006	0.0128	0.0116	-0.0141	0.0930	0.0006	0.0036	-0.0141
75	0	0	0	0.0003	0.0003	0.0138	0.0128	-0.0075	0.0751	0.0003	0.0042	-0.0075
75	0	0	0	0.0003	-0.0000	0.0158	0.0138	0.0000	0.0589	-0.0000	0.0042	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0047	-0.0000	0.2807	-0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0050	-0.0078	0.2741	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0058	-0.0146	0.2549	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0070	-0.0195	0.2258	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0085	-0.0221	0.1906	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0101	-0.0219	0.1536	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0116	-0.0191	0.1194	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0127	-0.0141	0.0918	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	0.0000	0.0000	0.0135	-0.0075	0.0740	0.0000	-0.0000	0.0000
75	0	0	0	0.0000	-0.0000	0.0000	0.0137	0.0000	0.0678	0.0000	-0.0000	0.0000



Table 2 continued, part 7 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
90	0	0	0.0000	-0.0000	0.0853	0.0000	0.0000	0.2992	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0916	0.0000	0.0000	0.2928	0.0000	0.0000	-0.0366
90	0	0	0.0000	-0.0000	0.1103	0.0000	0.0000	0.2742	0.0000	0.0000	-0.0687
90	0	0	0.0000	-0.0000	0.1388	0.0000	0.0000	0.2457	0.0000	0.0000	-0.0926
90	0	0	0.0000	-0.0000	0.1737	0.0000	0.0000	0.2108	0.0000	0.0000	-0.1053
90	0	0	0.0000	-0.0000	0.2108	0.0000	0.0000	0.1737	0.0000	-0.0000	-0.1053
90	0	0	0.0000	-0.0000	0.2457	0.0000	0.0000	0.1388	0.0000	-0.0000	-0.0926
90	0	0	0.0000	-0.0000	0.2742	0.0000	0.0000	0.1103	0.0000	-0.0000	-0.0687
90	0	0	0.0000	-0.0000	0.2928	0.0000	0.0000	0.0916	0.0000	-0.0000	-0.0366
90	0	0	0.0000	-0.0000	0.2992	0.0000	-0.0000	0.0853	-0.0000	0.0000	0.0000
90	0	10	0.0000	-0.0000	0.0784	0.0000	0.0000	0.2978	-0.0000	0.0000	0.0000
90	0	20	0.0000	-0.0000	0.0843	0.0000	0.0000	0.2913	0.0000	0.0000	-0.0348
90	0	30	0.0000	-0.0000	0.1011	0.0000	0.0000	0.2727	0.0000	0.0000	-0.0655
90	0	40	0.0000	-0.0000	0.1269	0.0000	0.0000	0.2442	0.0000	0.0000	-0.0882
90	0	50	0.0000	-0.0000	0.1585	0.0000	0.0000	0.2093	0.0000	0.0000	-0.1002
90	0	60	0.0000	-0.0000	0.1921	0.0000	0.0000	0.1721	0.0000	-0.0000	-0.1001
90	0	70	0.0000	-0.0000	0.2236	0.0000	0.0000	0.1373	0.0000	-0.0000	-0.0880
90	0	80	0.0000	-0.0000	0.2493	0.0000	0.0000	0.1089	0.0000	-0.0000	-0.0653
90	0	90	0.0000	-0.0000	0.2660	0.0000	0.0000	0.0903	0.0000	-0.0000	-0.0347
90	0	100	0.0000	-0.0000	0.2718	0.0000	-0.0000	0.0839	-0.0000	0.0000	0.0000
90	0	110	0.0000	-0.0000	0.0606	0.0000	0.0000	0.2940	-0.0000	0.0000	0.0000
90	0	120	0.0000	-0.0000	0.0649	0.0000	0.0000	0.2875	0.0000	0.0000	-0.0301
90	0	130	0.0000	-0.0000	0.0774	0.0000	0.0000	0.2688	0.0000	0.0000	-0.0564
90	0	140	0.0000	-0.0000	0.0966	0.0000	0.0000	0.2401	0.0000	0.0000	-0.0759
90	0	150	0.0000	-0.0000	0.1199	0.0000	0.0000	0.2051	0.0000	0.0000	-0.0861
90	0	160	0.0000	-0.0000	0.1447	0.0000	0.0000	0.1679	0.0000	-0.0000	-0.0860
90	0	170	0.0000	-0.0000	0.1678	0.0000	0.0000	0.1332	0.0000	-0.0000	-0.0754
90	0	180	0.0000	-0.0000	0.1866	0.0000	0.0000	0.1050	0.0000	-0.0000	-0.0559
90	0	190	0.0000	-0.0000	0.1989	0.0000	0.0000	0.0866	0.0000	-0.0000	-0.0297
90	0	200	0.0000	-0.0000	0.2031	0.0000	-0.0000	0.0802	-0.0000	0.0000	0.0000
90	0	210	0.0000	-0.0000	0.0382	0.0000	0.0000	0.2890	-0.0000	0.0000	0.0000
90	0	220	0.0000	-0.0000	0.0409	0.0000	0.0000	0.2824	0.0000	0.0000	-0.0233
90	0	230	0.0000	-0.0000	0.0483	0.0000	0.0000	0.2639	0.0000	0.0000	-0.0437
90	0	240	0.0000	-0.0000	0.0597	0.0000	0.0000	0.2347	0.0000	0.0000	-0.0587
90	0	250	0.0000	-0.0000	0.0736	0.0000	0.0000	0.1995	0.0000	0.0000	-0.0664
90	0	260	0.0000	-0.0000	0.0882	0.0000	0.0000	0.1624	0.0000	-0.0000	-0.0662
90	0	270	0.0000	-0.0000	0.1018	0.0000	0.0000	0.1279	0.0000	-0.0000	-0.0579
90	0	280	0.0000	-0.0000	0.1128	0.0000	0.0000	0.0999	0.0000	-0.0000	-0.0429
90	0	290	0.0000	-0.0000	0.1200	0.0000	0.0000	0.0817	0.0000	-0.0000	-0.0228
90	0	300	0.0000	-0.0000	0.1225	0.0000	-0.0000	0.0754	-0.0000	0.0000	0.0000
90	0	310	0.0000	-0.0000	0.0181	0.0000	0.0000	0.2842	0.0000	0.0000	0.0000
90	0	320	0.0000	-0.0000	0.0193	0.0000	0.0000	0.2775	0.0000	0.0000	-0.0156
90	0	330	0.0000	-0.0000	0.0226	0.0000	0.0000	0.2585	0.0000	0.0000	-0.0293
90	0	340	0.0000	-0.0000	0.0277	0.0000	0.0000	0.2295	0.0000	0.0000	-0.0393
90	0	350	0.0000	-0.0000	0.0339	0.0000	0.0000	0.1943	0.0000	0.0000	-0.0444
90	0	360	0.0000	-0.0000	0.0403	0.0000	0.0000	0.1572	0.0000	-0.0000	-0.0441
90	0	370	0.0000	-0.0000	0.0463	0.0000	0.0000	0.1229	0.0000	-0.0000	-0.0385
90	0	380	0.0000	-0.0000	0.0511	0.0000	0.0000	0.0951	0.0000	-0.0000	-0.0285
90	0	390	0.0000	-0.0000	0.0542	0.0000	0.0000	0.0771	0.0000	-0.0000	-0.0151
90	0	400	0.0000	-0.0000	0.0553	0.0000	-0.0000	0.0709	-0.0000	0.0000	0.0000
90	0	410	0.0000	-0.0000	0.0047	0.0000	0.0000	0.2807	-0.0000	0.0000	0.0000
90	0	420	0.0000	-0.0000	0.0050	0.0000	0.0000	0.2741	0.0000	0.0000	-0.0078
90	0	430	0.0000	-0.0000	0.0058	0.0000	0.0000	0.2549	0.0000	0.0000	-0.0146
90	0	440	0.0000	-0.0000	0.0070	0.0000	0.0000	0.2258	0.0000	0.0000	-0.0195
90	0	450	0.0000	-0.0000	0.0085	0.0000	0.0000	0.1906	0.0000	0.0000	-0.0221
90	0	460	0.0000	-0.0000	0.0101	0.0000	0.0000	0.1536	0.0000	-0.0000	-0.0219
90	0	470	0.0000	-0.0000	0.0116	0.0000	0.0000	0.1174	0.0000	-0.0000	-0.0191
90	0	480	0.0000	-0.0000	0.0127	0.0000	0.0000	0.0916	0.0000	-0.0000	-0.0141
90	0	490	0.0000	-0.0000	0.0135	0.0000	0.0000	0.0740	0.0000	-0.0000	-0.0075
90	0	500	0.0000	-0.0000	0.0137	0.0000	-0.0000	0.0678	-0.0000	0.0000	0.0000
90	0	510	0.0000	-0.0000	0.0000	0.0000	0.0000	0.2795	-0.0000	0.0000	0.0000
90	0	520	0.0000	-0.0000	0.0000	0.0000	0.0000	0.2728	-0.0000	0.0000	0.0000
90	0	530	0.0000	-0.0000	0.0000	0.0000	0.0000	0.2536	-0.0000	0.0000	0.0000
90	0	540	0.0000	-0.0000	0.0000	0.0000	0.0000	0.2245	-0.0000	0.0000	0.0000
90	0	550	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1893	-0.0000	-0.0000	0.0000
90	0	560	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1523	-0.0000	-0.0000	0.0000
90	0	570	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1181	-0.0000	0.0000	0.0000
90	0	580	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0906	-0.0000	0.0000	0.0000
90	0	590	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0729	-0.0000	0.0000	0.0000
90	0	600	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0667	0.0000	0.0000	-0.0000

TABLE 3. PARAMETERS  $\sigma_i$ ,  $i = 1, 2, \dots, 9$ , NORMALIZED TO  $\lambda^2$   
FOR SCATTERING FROM A FULL-WAVELENGTH DIPOLE  
( $L = \lambda$ ). ANGLES  $\theta_1$ ,  $\theta_2$ , AND  $\theta_\phi$  SHOWN IN DEGREES.

$\theta_1$	$\theta_2$	$\theta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
0	0	0	0.0341	0.0000	0.0114	0.0114	-0.0000	0.0341	-0.0000	-0.0114	0.0000
0	0	10	0.0334	0.0039	0.0120	0.0120	-0.0039	0.0334	0.0039	-0.0107	-0.0039
0	0	20	0.0314	0.0073	0.0140	0.0140	-0.0073	0.0314	0.0073	-0.0087	-0.0073
0	0	30	0.0284	0.0098	0.0170	0.0170	-0.0098	0.0284	0.0098	-0.0057	-0.0098
0	0	40	0.0247	0.0112	0.0207	0.0207	-0.0112	0.0247	0.0112	-0.0020	-0.0112
0	0	50	0.0207	0.0112	0.0247	0.0247	-0.0112	0.0207	0.0112	0.0020	-0.0112
0	0	60	0.0170	0.0098	0.0284	0.0284	-0.0098	0.0170	0.0098	0.0057	-0.0098
0	0	70	0.0140	0.0073	0.0314	0.0314	-0.0073	0.0140	0.0073	0.0087	-0.0073
0	0	80	0.0120	0.0039	0.0334	0.0334	-0.0039	0.0120	0.0039	0.0107	-0.0039
0	0	90	0.0114	-0.0000	0.0341	0.0341	-0.0000	0.0114	-0.0000	0.0114	0.0000
0	10	0	0.0310	0.0070	0.0104	0.0112	-0.0000	0.0339	-0.0000	-0.0106	0.0000
0	10	10	0.0304	0.0033	0.0111	0.0119	-0.0039	0.0332	0.0037	-0.0101	0.0037
0	10	20	0.0286	0.0066	0.0128	0.0138	-0.0073	0.0312	0.0069	-0.0083	0.0069
0	10	30	0.0258	0.0089	0.0156	0.0169	-0.0098	0.0282	0.0094	-0.0054	0.0094
0	10	40	0.0223	0.0101	0.0189	0.0206	-0.0112	0.0243	0.0106	-0.0019	0.0106
0	10	50	0.0189	0.0101	0.0223	0.0243	-0.0112	0.0206	0.0106	0.0019	0.0106
0	10	60	0.0156	0.0089	0.0258	0.0282	-0.0098	0.0169	0.0094	0.0054	0.0094
0	10	70	0.0128	0.0066	0.0286	0.0312	-0.0073	0.0138	0.0069	0.0083	0.0069
0	10	80	0.0111	0.0033	0.0304	0.0332	-0.0039	0.0119	0.0037	0.0101	0.0037
0	10	90	0.0104	-0.0000	0.0310	0.0339	-0.0000	0.0112	-0.0000	0.0103	0.0000
0	20	0	0.0232	0.0000	0.0080	0.0107	-0.0000	0.0334	-0.0000	-0.0093	0.0000
0	20	10	0.0217	0.0026	0.0083	0.0114	-0.0039	0.0327	0.0032	-0.0087	0.0032
0	20	20	0.0214	0.0049	0.0098	0.0134	-0.0073	0.0308	0.0060	-0.0071	0.0060
0	20	30	0.0214	0.0073	0.0118	0.0164	-0.0098	0.0277	0.0080	-0.0046	0.0080
0	20	40	0.0214	0.0098	0.0143	0.0201	-0.0112	0.0240	0.0091	-0.0016	0.0091
0	20	50	0.0214	0.0118	0.0169	0.0240	-0.0112	0.0201	0.0091	0.0016	0.0091
0	20	60	0.0214	0.0143	0.0194	0.0277	-0.0098	0.0164	0.0080	0.0046	0.0080
0	20	70	0.0214	0.0169	0.0214	0.0308	-0.0073	0.0134	0.0060	0.0071	0.0060
0	20	80	0.0214	0.0194	0.0227	0.0327	-0.0039	0.0114	0.0032	0.0087	0.0032
0	20	90	0.0214	-0.0000	0.0232	0.0334	-0.0000	0.0107	-0.0000	0.0093	0.0000
0	30	0	0.0140	0.0000	0.0051	0.0101	-0.0000	0.0338	-0.0000	-0.0071	0.0000
0	30	10	0.0137	0.0013	0.0053	0.0108	-0.0039	0.0321	0.0024	-0.0067	0.0024
0	30	20	0.0130	0.0029	0.0061	0.0123	-0.0073	0.0301	0.0046	-0.0053	0.0046
0	30	30	0.0118	0.0039	0.0073	0.0138	-0.0098	0.0271	0.0062	-0.0033	0.0062
0	30	40	0.0103	0.0044	0.0088	0.0158	-0.0112	0.0234	0.0070	-0.0012	0.0070
0	30	50	0.0088	0.0044	0.0103	0.0201	-0.0112	0.0193	0.0070	0.0012	0.0070
0	30	60	0.0073	0.0039	0.0118	0.0240	-0.0098	0.0158	0.0062	0.0033	0.0062
0	30	70	0.0061	0.0029	0.0130	0.0271	-0.0073	0.0138	0.0046	0.0053	0.0046
0	30	80	0.0051	0.0013	0.0137	0.0301	-0.0039	0.0108	0.0024	0.0067	0.0024
0	30	90	0.0043	-0.0000	0.0140	0.0327	-0.0000	0.0101	-0.0000	0.0071	0.0000
0	40	0	0.0063	0.0000	0.0024	0.0106	-0.0000	0.0322	-0.0000	-0.0048	0.0000
0	40	10	0.0059	0.0007	0.0023	0.0110	-0.0039	0.0313	0.0016	-0.0043	0.0016
0	40	20	0.0053	0.0013	0.0028	0.0123	-0.0073	0.0293	0.0031	-0.0037	0.0031
0	40	30	0.0047	0.0017	0.0034	0.0138	-0.0098	0.0263	0.0041	-0.0024	0.0041
0	40	40	0.0040	0.0019	0.0040	0.0158	-0.0112	0.0228	0.0047	-0.0008	0.0047
0	40	50	0.0034	0.0017	0.0047	0.0201	-0.0112	0.0189	0.0047	0.0008	0.0047
0	40	60	0.0028	0.0013	0.0053	0.0240	-0.0098	0.0158	0.0031	0.0024	0.0031
0	40	70	0.0023	0.0007	0.0061	0.0271	-0.0073	0.0138	0.0016	0.0043	0.0016
0	40	80	0.0019	0.0000	0.0063	0.0301	-0.0039	0.0108	0.0000	0.0067	0.0000
0	40	90	0.0013	-0.0000	0.0066	0.0327	-0.0000	0.0101	-0.0000	0.0071	0.0000
0	50	0	0.0013	0.0000	0.0006	0.0098	-0.0000	0.0318	-0.0000	-0.0008	0.0000
0	50	10	0.0013	0.0000	0.0006	0.0106	-0.0039	0.0311	0.0008	-0.0008	0.0008
0	50	20	0.0013	0.0000	0.0007	0.0118	-0.0073	0.0291	0.0015	-0.0018	0.0015
0	50	30	0.0012	0.0004	0.0009	0.0148	-0.0098	0.0261	0.0021	-0.0012	0.0021
0	50	40	0.0010	0.0005	0.0010	0.0183	-0.0111	0.0224	0.0023	-0.0004	0.0023
0	50	50	0.0009	0.0004	0.0012	0.0224	-0.0111	0.0183	0.0023	0.0004	0.0023
0	50	60	0.0007	0.0003	0.0013	0.0261	-0.0098	0.0148	0.0021	0.0012	0.0021
0	50	70	0.0006	0.0002	0.0013	0.0291	-0.0073	0.0118	0.0015	0.0018	0.0015
0	50	80	0.0006	-0.0000	0.0016	0.0311	-0.0039	0.0098	0.0008	0.0024	0.0008
0	50	90	0.0000	0.0000	0.0000	0.0318	-0.0000	0.0092	-0.0000	0.0024	0.0000
0	60	0	0.0000	0.0000	0.0000	0.0090	-0.0000	0.0316	-0.0000	0.0000	0.0000
0	60	10	0.0000	0.0000	0.0000	0.0097	-0.0039	0.0309	0.0000	0.0000	0.0000
0	60	20	0.0000	0.0000	0.0000	0.0117	-0.0073	0.0290	0.0000	0.0000	0.0000
0	60	30	0.0000	0.0000	0.0000	0.0147	-0.0098	0.0260	0.0000	0.0000	0.0000
0	60	40	0.0000	0.0000	0.0000	0.0183	-0.0111	0.0223	0.0000	0.0000	0.0000
0	60	50	0.0000	0.0000	0.0000	0.0223	-0.0111	0.0183	0.0000	0.0000	0.0000
0	60	60	0.0000	0.0000	0.0000	0.0260	-0.0098	0.0147	0.0000	0.0000	0.0000
0	60	70	0.0000	0.0000	0.0000	0.0290	-0.0073	0.0117	0.0000	0.0000	0.0000
0	60	80	0.0000	0.0000	0.0000	0.0309	-0.0039	0.0097	0.0000	0.0000	0.0000
0	60	90	0.0000	-0.0000	0.0000	0.0316	-0.0000	0.0090	0.0000	0.0000	0.0000

Table 3 continued, part 2 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
13.0	0.0	0.0	0.0310	0.0000	0.0112	0.0104	-0.0000	0.0339	-0.0000	-0.0108	0.0000
13.0	0.0	0.0	0.0304	0.0037	0.0119	0.0111	-0.0037	0.0332	0.0033	-0.0101	-0.0039
13.0	0.0	0.0	0.0286	0.0069	0.0138	0.0128	-0.0069	0.0312	0.0066	-0.0083	-0.0073
13.0	0.0	0.0	0.0258	0.0094	0.0169	0.0136	-0.0094	0.0282	0.0089	-0.0054	-0.0098
13.0	0.0	0.0	0.0225	0.0106	0.0206	0.0189	-0.0106	0.0245	0.0101	-0.0019	-0.0112
13.0	0.0	0.0	0.0189	0.0106	0.0243	0.0225	-0.0106	0.0206	0.0101	0.0019	-0.0112
13.0	0.0	0.0	0.0156	0.0094	0.0282	0.0258	-0.0094	0.0169	0.0089	0.0034	-0.0098
13.0	0.0	0.0	0.0128	0.0069	0.0312	0.0286	-0.0069	0.0138	0.0066	0.0083	-0.0073
13.0	0.0	0.0	0.0111	0.0037	0.0332	0.0304	-0.0037	0.0119	0.0033	0.0101	-0.0039
13.0	0.0	0.0	0.0104	-0.0000	0.0339	0.0310	0.0000	0.0112	-0.0000	0.0108	0.0000
13.0	0.0	0.0	0.0282	0.0000	0.0103	0.0103	-0.0000	0.0337	-0.0000	-0.0103	0.0000
13.0	0.0	0.0	0.0276	0.0033	0.0109	0.0109	-0.0037	0.0330	0.0033	-0.0097	0.0037
13.0	0.0	0.0	0.0260	0.0063	0.0127	0.0127	-0.0069	0.0311	0.0063	-0.0079	0.0069
13.0	0.0	0.0	0.0235	0.0085	0.0154	0.0154	-0.0094	0.0260	0.0085	-0.0051	0.0094
13.0	0.0	0.0	0.0205	0.0096	0.0188	0.0188	-0.0106	0.0243	0.0096	-0.0018	0.0106
13.0	0.0	0.0	0.0173	0.0096	0.0223	0.0223	-0.0106	0.0204	0.0096	0.0018	-0.0106
13.0	0.0	0.0	0.0142	0.0083	0.0257	0.0257	-0.0094	0.0167	0.0083	0.0051	-0.0094
13.0	0.0	0.0	0.0118	0.0063	0.0284	0.0284	-0.0069	0.0137	0.0063	0.0079	-0.0069
13.0	0.0	0.0	0.0101	0.0033	0.0302	0.0302	-0.0037	0.0117	0.0033	0.0103	-0.0037
13.0	0.0	0.0	0.0096	-0.0000	0.0308	0.0308	0.0000	0.0110	-0.0000	0.0103	0.0000
13.0	0.0	0.0	0.0211	0.0000	0.0079	0.0098	-0.0000	0.0333	0.0000	-0.0088	0.0000
13.0	0.0	0.0	0.0207	0.0023	0.0084	0.0103	-0.0037	0.0326	0.0024	-0.0083	0.0032
13.0	0.0	0.0	0.0195	0.0046	0.0097	0.0122	-0.0069	0.0306	0.0049	-0.0068	0.0060
13.0	0.0	0.0	0.0176	0.0062	0.0117	0.0150	-0.0094	0.0276	0.0073	-0.0044	0.0080
13.0	0.0	0.0	0.0154	0.0071	0.0142	0.0183	-0.0106	0.0239	0.0083	-0.0013	0.0091
13.0	0.0	0.0	0.0130	0.0071	0.0168	0.0219	-0.0106	0.0199	0.0083	0.0013	-0.0091
13.0	0.0	0.0	0.0108	0.0062	0.0193	0.0252	-0.0093	0.0162	0.0073	0.0044	-0.0080
13.0	0.0	0.0	0.0090	0.0046	0.0213	0.0280	-0.0069	0.0132	0.0054	0.0068	-0.0060
13.0	0.0	0.0	0.0078	0.0023	0.0225	0.0298	-0.0037	0.0112	0.0049	0.0093	-0.0032
13.0	0.0	0.0	0.0074	-0.0000	0.0231	0.0304	0.0000	0.0105	-0.0000	0.0088	0.0000
13.0	0.0	0.0	0.0127	0.0000	0.0050	0.0093	-0.0000	0.0326	-0.0000	-0.0068	0.0000
13.0	0.0	0.0	0.0123	0.0013	0.0052	0.0099	-0.0037	0.0319	0.0022	-0.0064	0.0024
13.0	0.0	0.0	0.0118	0.0027	0.0060	0.0117	-0.0069	0.0300	0.0042	-0.0052	0.0046
13.0	0.0	0.0	0.0107	0.0037	0.0072	0.0144	-0.0093	0.0270	0.0056	-0.0034	0.0062
13.0	0.0	0.0	0.0094	0.0042	0.0087	0.0178	-0.0106	0.0233	0.0064	-0.0012	0.0070
13.0	0.0	0.0	0.0080	0.0042	0.0102	0.0213	-0.0106	0.0193	0.0064	0.0012	-0.0070
13.0	0.0	0.0	0.0067	0.0037	0.0117	0.0247	-0.0093	0.0156	0.0056	0.0034	-0.0062
13.0	0.0	0.0	0.0056	0.0027	0.0129	0.0274	-0.0069	0.0126	0.0042	0.0052	-0.0046
13.0	0.0	0.0	0.0049	0.0013	0.0137	0.0292	-0.0037	0.0106	0.0022	0.0064	-0.0024
13.0	0.0	0.0	0.0046	-0.0000	0.0139	0.0298	0.0000	0.0099	-0.0000	0.0068	0.0000
13.0	0.0	0.0	0.0038	0.0000	0.0024	0.0088	-0.0000	0.0320	-0.0000	-0.0043	0.0000
13.0	0.0	0.0	0.0037	0.0006	0.0025	0.0094	-0.0037	0.0314	0.0013	-0.0043	0.0016
13.0	0.0	0.0	0.0033	0.0012	0.0028	0.0112	-0.0069	0.0294	0.0028	-0.0035	0.0031
13.0	0.0	0.0	0.0049	0.0016	0.0033	0.0139	-0.0093	0.0264	0.0037	-0.0023	0.0041
13.0	0.0	0.0	0.0043	0.0018	0.0040	0.0172	-0.0106	0.0227	0.0043	-0.0008	0.0047
13.0	0.0	0.0	0.0037	0.0018	0.0047	0.0208	-0.0106	0.0187	0.0042	0.0008	-0.0047
13.0	0.0	0.0	0.0031	0.0016	0.0053	0.0241	-0.0093	0.0150	0.0037	0.0023	-0.0041
13.0	0.0	0.0	0.0026	0.0012	0.0058	0.0269	-0.0069	0.0120	0.0028	0.0035	-0.0031
13.0	0.0	0.0	0.0023	0.0006	0.0062	0.0286	-0.0037	0.0101	0.0013	0.0043	-0.0016
13.0	0.0	0.0	0.0022	-0.0000	0.0063	0.0293	0.0000	0.0094	-0.0000	0.0043	0.0000
13.0	0.0	0.0	0.0014	0.0000	0.0066	0.0084	-0.0000	0.0316	-0.0000	-0.0023	0.0000
13.0	0.0	0.0	0.0014	0.0002	0.0066	0.0090	-0.0037	0.0309	0.0007	-0.0021	0.0008
13.0	0.0	0.0	0.0013	0.0003	0.0067	0.0108	-0.0069	0.0290	0.0014	-0.0017	0.0013
13.0	0.0	0.0	0.0012	0.0004	0.0068	0.0135	-0.0093	0.0259	0.0019	-0.0011	0.0021
13.0	0.0	0.0	0.0011	0.0005	0.0010	0.0169	-0.0106	0.0223	0.0021	-0.0004	0.0023
13.0	0.0	0.0	0.0009	0.0003	0.0012	0.0204	-0.0106	0.0183	0.0021	0.0004	-0.0023
13.0	0.0	0.0	0.0008	0.0004	0.0013	0.0238	-0.0093	0.0146	0.0019	0.0011	-0.0020
13.0	0.0	0.0	0.0007	0.0003	0.0015	0.0269	-0.0069	0.0116	0.0014	0.0017	-0.0013
13.0	0.0	0.0	0.0006	0.0002	0.0015	0.0282	-0.0037	0.0097	0.0007	0.0021	-0.0008
13.0	0.0	0.0	0.0006	-0.0000	0.0016	0.0289	0.0000	0.0090	-0.0000	0.0023	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0083	-0.0000	0.0313	0.0000	-0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0089	-0.0037	0.0308	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0107	-0.0069	0.0288	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0134	-0.0093	0.0258	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0167	-0.0106	0.0221	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0203	-0.0106	0.0182	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0236	-0.0093	0.0145	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0263	-0.0069	0.0113	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	0.0000	0.0000	0.0281	-0.0037	0.0093	-0.0000	0.0000	0.0000
13.0	0.0	0.0	0.0000	-0.0000	0.0000	0.0287	0.0000	0.0089	0.0000	-0.0000	0.0000

Table 3 continued, part 3 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
30	0	0	0.0232	0.0000	0.0107	0.0080	-0.0000	0.0334	-0.0000	-0.0093	0.0000
30	0	0	0.0227	0.0032	0.0114	0.0085	-0.0032	0.0327	0.0026	-0.0087	-0.0039
30	0	0	0.0214	0.0060	0.0134	0.0098	-0.0060	0.0308	0.0049	-0.0071	-0.0073
30	0	0	0.0194	0.0080	0.0164	0.0118	-0.0080	0.0277	0.0066	-0.0046	-0.0098
30	0	0	0.0169	0.0091	0.0201	0.0143	-0.0091	0.0240	0.0075	-0.0016	-0.0112
30	0	0	0.0143	0.0091	0.0240	0.0169	-0.0091	0.0201	0.0075	0.0016	-0.0112
30	0	0	0.0118	0.0080	0.0277	0.0194	-0.0080	0.0164	0.0066	0.0046	-0.0098
30	0	0	0.0098	0.0060	0.0308	0.0214	-0.0060	0.0134	0.0049	0.0071	-0.0073
30	0	0	0.0085	0.0032	0.0327	0.0227	-0.0032	0.0114	0.0026	0.0087	-0.0039
30	0	0	0.0080	-0.0000	0.0334	0.0232	-0.0000	0.0107	-0.0026	0.0093	0.0000
30	0	0	0.0211	0.0000	0.0098	0.0079	-0.0000	0.0333	-0.0000	-0.0088	0.0000
30	0	15	0.0207	0.0029	0.0103	0.0084	-0.0032	0.0326	0.0023	-0.0083	-0.0037
30	0	15	0.0195	0.0054	0.0122	0.0097	-0.0060	0.0306	0.0046	-0.0068	-0.0069
30	0	15	0.0176	0.0073	0.0150	0.0117	-0.0080	0.0276	0.0062	-0.0044	-0.0094
30	0	15	0.0154	0.0083	0.0183	0.0142	-0.0091	0.0239	0.0071	-0.0011	-0.0106
30	0	15	0.0130	0.0083	0.0219	0.0168	-0.0091	0.0199	0.0071	0.0011	-0.0106
30	0	15	0.0108	0.0073	0.0253	0.0193	-0.0080	0.0162	0.0062	0.0011	-0.0093
30	0	15	0.0090	0.0054	0.0280	0.0213	-0.0060	0.0132	0.0046	0.0026	-0.0069
30	0	15	0.0078	0.0029	0.0298	0.0226	-0.0032	0.0112	0.0023	0.0044	-0.0037
30	0	15	0.0074	-0.0000	0.0304	0.0231	-0.0000	0.0105	-0.0023	0.0053	0.0000
30	0	15	0.0158	0.0000	0.0074	0.0074	-0.0000	0.0328	-0.0000	-0.0066	0.0000
30	0	15	0.0155	0.0021	0.0080	0.0080	-0.0032	0.0321	0.0021	-0.0066	-0.0032
30	0	15	0.0144	0.0040	0.0094	0.0094	-0.0060	0.0301	0.0040	-0.0044	-0.0060
30	0	15	0.0132	0.0054	0.0114	0.0114	-0.0080	0.0271	0.0054	-0.0026	-0.0080
30	0	15	0.0114	0.0061	0.0139	0.0139	-0.0091	0.0234	0.0061	-0.0011	-0.0091
30	0	15	0.0098	0.0061	0.0165	0.0165	-0.0091	0.0193	0.0061	0.0011	-0.0091
30	0	15	0.0082	0.0054	0.0189	0.0189	-0.0080	0.0158	0.0054	0.0026	-0.0080
30	0	15	0.0067	0.0040	0.0210	0.0210	-0.0060	0.0127	0.0040	0.0044	-0.0060
30	0	15	0.0060	0.0021	0.0223	0.0223	-0.0032	0.0108	0.0021	0.0058	-0.0032
30	0	15	0.0057	0.0000	0.0227	0.0227	-0.0000	0.0101	-0.0000	0.0074	0.0000
30	0	15	0.0053	-0.0000	0.0048	0.0072	-0.0000	0.0322	-0.0000	-0.0059	0.0000
30	0	15	0.0053	0.0013	0.0050	0.0072	-0.0032	0.0315	0.0013	-0.0055	-0.0025
30	0	15	0.0088	0.0024	0.0058	0.0079	-0.0060	0.0295	0.0024	-0.0043	-0.0046
30	0	15	0.0080	0.0032	0.0070	0.0110	-0.0080	0.0265	0.0032	-0.0029	-0.0062
30	0	15	0.0071	0.0036	0.0085	0.0134	-0.0091	0.0228	0.0036	-0.0010	-0.0070
30	0	15	0.0060	0.0036	0.0100	0.0161	-0.0091	0.0189	0.0047	0.0010	-0.0070
30	0	15	0.0051	0.0032	0.0113	0.0185	-0.0080	0.0152	0.0041	0.0024	-0.0062
30	0	15	0.0043	0.0023	0.0127	0.0203	-0.0059	0.0122	0.0031	0.0043	-0.0046
30	0	15	0.0037	0.0012	0.0134	0.0218	-0.0032	0.0102	0.0016	0.0055	-0.0024
30	0	15	0.0036	-0.0000	0.0137	0.0223	-0.0000	0.0093	-0.0000	0.0058	0.0000
30	0	15	0.0043	0.0000	0.0123	0.0068	-0.0000	0.0316	-0.0000	-0.0039	0.0000
30	0	15	0.0042	0.0006	0.0074	0.0072	-0.0032	0.0309	0.0011	-0.0037	-0.0016
30	0	15	0.0040	0.0010	0.0027	0.0086	-0.0060	0.0289	0.0021	-0.0030	-0.0031
30	0	15	0.0037	0.0014	0.0033	0.0106	-0.0080	0.0259	0.0028	-0.0019	-0.0041
30	0	15	0.0032	0.0016	0.0039	0.0130	-0.0091	0.0222	0.0031	-0.0007	-0.0047
30	0	15	0.0028	0.0016	0.0046	0.0157	-0.0091	0.0183	0.0031	0.0007	-0.0047
30	0	15	0.0023	0.0014	0.0052	0.0181	-0.0080	0.0146	0.0027	0.0020	-0.0041
30	0	15	0.0020	0.0010	0.0057	0.0201	-0.0059	0.0116	0.0020	0.0030	-0.0031
30	0	15	0.0018	0.0005	0.0061	0.0214	-0.0031	0.0097	0.0011	0.0037	-0.0016
30	0	15	0.0017	-0.0000	0.0062	0.0219	-0.0000	0.0090	-0.0000	0.0039	0.0000
30	0	15	0.0011	0.0000	0.0066	0.0065	-0.0000	0.0312	-0.0000	-0.0019	0.0000
30	0	15	0.0010	0.0001	0.0066	0.0070	-0.0032	0.0305	0.0003	-0.0018	-0.0008
30	0	15	0.0009	0.0003	0.0007	0.0083	-0.0060	0.0285	0.0010	-0.0015	-0.0015
30	0	15	0.0004	0.0003	0.0008	0.0103	-0.0080	0.0255	0.0014	-0.0010	-0.0021
30	0	15	0.0007	0.0004	0.0010	0.0128	-0.0091	0.0218	0.0014	-0.0003	-0.0023
30	0	15	0.0006	0.0003	0.0011	0.0154	-0.0091	0.0179	0.0016	0.0003	-0.0023
30	0	15	0.0005	0.0003	0.0014	0.0178	-0.0080	0.0142	0.0014	0.0010	-0.0020
30	0	15	0.0005	0.0001	0.0015	0.0198	-0.0059	0.0112	0.0010	0.0015	-0.0015
30	0	15	0.0004	-0.0000	0.0015	0.0211	-0.0031	0.0093	0.0003	0.0018	-0.0008
30	0	15	0.0000	0.0000	0.0015	0.0216	-0.0000	0.0086	-0.0000	0.0019	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0064	-0.0000	0.0311	-0.0000	-0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0069	-0.0032	0.0304	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0082	-0.0060	0.0284	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0102	-0.0080	0.0254	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0127	-0.0091	0.0217	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0153	-0.0091	0.0177	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0177	-0.0080	0.0141	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0197	-0.0059	0.0111	-0.0000	0.0000	0.0000
30	0	15	0.0000	0.0000	0.0000	0.0210	-0.0031	0.0091	-0.0000	0.0000	0.0000
30	0	15	0.0000	-0.0000	0.0000	0.0215	0.0000	0.0085	0.0000	-0.0000	-0.0000

Table 3 continued, part 4 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
45	0	0	0.0140	0.0000	0.0101	0.0031	-0.0000	0.0328	-0.0000	-0.0071	0.0000
45	0	0	0.0137	0.0024	0.0108	0.0053	-0.0024	0.0321	0.0015	-0.0067	-0.0039
45	0	0	0.0130	0.0046	0.0128	0.0061	-0.0046	0.0301	0.0029	-0.0059	-0.0073
45	0	0	0.0118	0.0062	0.0158	0.0073	-0.0062	0.0271	0.0039	-0.0036	-0.0098
45	0	0	0.0103	0.0070	0.0195	0.0088	-0.0070	0.0234	0.0044	-0.0012	-0.0112
45	0	0	0.0088	0.0070	0.0234	0.0103	-0.0070	0.0195	0.0044	0.0012	-0.0112
45	0	0	0.0073	0.0062	0.0271	0.0116	-0.0062	0.0158	0.0039	0.0036	-0.0098
45	0	0	0.0061	0.0046	0.0301	0.0130	-0.0046	0.0128	0.0029	0.0059	-0.0073
45	0	0	0.0053	0.0024	0.0321	0.0137	-0.0024	0.0108	0.0015	0.0067	-0.0039
45	0	0	0.0051	-0.0000	0.0328	0.0140	-0.0000	0.0101	-0.0000	0.0071	0.0000
45	0	0	0.0127	0.0000	0.0093	0.0050	-0.0000	0.0326	-0.0000	-0.0068	0.0000
45	0	0	0.0123	0.0022	0.0099	0.0052	-0.0024	0.0317	0.0013	-0.0064	-0.0037
45	0	0	0.0118	0.0042	0.0117	0.0060	-0.0046	0.0300	0.0027	-0.0052	-0.0069
45	0	0	0.0107	0.0056	0.0144	0.0072	-0.0062	0.0270	0.0037	-0.0034	-0.0093
45	0	0	0.0094	0.0064	0.0178	0.0087	-0.0070	0.0233	0.0042	-0.0012	-0.0106
45	0	0	0.0080	0.0064	0.0213	0.0102	-0.0070	0.0193	0.0042	0.0012	-0.0106
45	0	0	0.0067	0.0056	0.0247	0.0117	-0.0062	0.0156	0.0037	0.0034	-0.0093
45	0	0	0.0056	0.0042	0.0274	0.0129	-0.0046	0.0126	0.0027	0.0052	-0.0069
45	0	0	0.0049	0.0022	0.0292	0.0137	-0.0024	0.0106	0.0013	0.0064	-0.0037
45	0	0	0.0046	-0.0000	0.0298	0.0139	-0.0000	0.0099	-0.0000	0.0068	0.0000
45	0	0	0.0043	0.0000	0.0278	0.0048	-0.0000	0.0322	-0.0000	-0.0059	0.0000
45	0	0	0.0033	0.0016	0.0276	0.0050	-0.0023	0.0319	0.0013	-0.0059	-0.0032
45	0	0	0.0088	0.0031	0.0089	0.0058	-0.0046	0.0295	0.0024	-0.0045	-0.0060
45	0	0	0.0080	0.0041	0.0110	0.0070	-0.0062	0.0265	0.0032	-0.0029	-0.0080
45	0	0	0.0071	0.0047	0.0134	0.0085	-0.0070	0.0228	0.0036	-0.0010	-0.0091
45	0	0	0.0060	0.0047	0.0161	0.0100	-0.0070	0.0199	0.0036	0.0010	-0.0091
45	0	0	0.0051	0.0041	0.0185	0.0119	-0.0062	0.0152	0.0032	0.0045	-0.0080
45	0	0	0.0043	0.0031	0.0205	0.012	-0.0046	0.0122	0.0023	0.0045	-0.0059
45	0	0	0.0037	0.0016	0.0218	0.0134	-0.0024	0.0102	0.0012	0.0053	-0.0032
45	0	0	0.0036	-0.0000	0.0223	0.0137	-0.0000	0.0095	-0.0000	0.0058	0.0000
45	0	0	0.0038	0.0000	0.0045	0.0045	-0.0000	0.0316	-0.0000	-0.0045	0.0000
45	0	0	0.0037	0.0010	0.0048	0.0043	-0.0023	0.0309	0.0010	-0.0042	-0.0023
45	0	0	0.0033	0.0018	0.0056	0.0056	-0.0046	0.0289	0.0018	-0.0035	-0.0046
45	0	0	0.0049	0.0024	0.0068	0.0068	-0.0062	0.0259	0.0024	-0.0022	-0.0062
45	0	0	0.0043	0.0028	0.0082	0.0082	-0.0070	0.0222	0.0028	-0.0008	-0.0070
45	0	0	0.0037	0.0028	0.0098	0.0098	-0.0070	0.0183	0.0028	0.0008	-0.0070
45	0	0	0.0031	0.0024	0.0112	0.0112	-0.0062	0.0146	0.0024	0.0023	-0.0062
45	0	0	0.0026	0.0018	0.0124	0.0124	-0.0046	0.0116	0.0018	0.0034	-0.0046
45	0	0	0.0023	0.0010	0.0132	0.0132	-0.0024	0.0096	0.0010	0.0042	-0.0024
45	0	0	0.0022	-0.0000	0.0134	0.0134	-0.0000	0.0090	-0.0000	0.0045	0.0000
45	0	0	0.0026	0.0000	0.0021	0.0043	-0.0000	0.0311	-0.0000	-0.0030	0.0000
45	0	0	0.0024	0.0004	0.0023	0.0045	-0.0023	0.0304	0.0006	-0.0028	-0.0016
45	0	0	0.0024	0.0008	0.0026	0.0053	-0.0046	0.0284	0.0012	-0.0023	-0.0031
45	0	0	0.0022	0.0011	0.0031	0.0065	-0.0062	0.0253	0.0016	-0.0013	-0.0041
45	0	0	0.0020	0.0012	0.0038	0.0080	-0.0070	0.0216	0.0019	-0.0003	-0.0047
45	0	0	0.0017	0.0012	0.0045	0.0095	-0.0070	0.0177	0.0018	0.0003	-0.0047
45	0	0	0.0014	0.0011	0.0051	0.0110	-0.0061	0.0140	0.0016	0.0015	-0.0041
45	0	0	0.0012	0.0008	0.0056	0.0122	-0.0045	0.0111	0.0012	0.0023	-0.0030
45	0	0	0.0011	0.0004	0.0060	0.0129	-0.0024	0.0091	0.0006	0.0028	-0.0016
45	0	0	0.0011	-0.0000	0.0061	0.0132	-0.0000	0.0085	-0.0000	0.0030	0.0000
45	0	0	0.0007	0.0000	0.0005	0.0041	-0.0000	0.0307	-0.0000	-0.0015	0.0000
45	0	0	0.0006	0.0001	0.0006	0.0044	-0.0023	0.0300	0.0003	-0.0014	-0.0008
45	0	0	0.0006	0.0002	0.0007	0.0052	-0.0046	0.0280	0.0006	-0.0011	-0.0015
45	0	0	0.0006	0.0003	0.0008	0.0064	-0.0062	0.0249	0.0008	-0.0007	-0.0021
45	0	0	0.0005	0.0003	0.0010	0.0078	-0.0070	0.0212	0.0009	-0.0002	-0.0023
45	0	0	0.0004	0.0003	0.0011	0.0094	-0.0070	0.0173	0.0009	0.0003	-0.0023
45	0	0	0.0004	0.0003	0.0013	0.0108	-0.0061	0.0136	0.0008	0.0008	-0.0020
45	0	0	0.0003	0.0002	0.0014	0.0120	-0.0045	0.0107	0.0006	0.0011	-0.0015
45	0	0	0.0003	0.0001	0.0015	0.0127	-0.0024	0.0088	0.0003	0.0014	-0.0008
45	0	0	0.0003	-0.0000	0.0015	0.0130	-0.0000	0.0081	-0.0000	0.0015	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0040	-0.0000	0.0305	0.0000	0.0000	-0.0000
45	0	0	0.0000	0.0000	0.0000	0.0043	-0.0023	0.0298	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0051	-0.0046	0.0278	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0063	-0.0062	0.0248	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0078	-0.0070	0.0211	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0093	-0.0070	0.0172	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0108	-0.0061	0.0135	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0119	-0.0045	0.0106	-0.0000	0.0000	0.0000
45	0	0	0.0000	0.0000	0.0000	0.0127	-0.0024	0.0086	-0.0000	0.0000	0.0000
45	0	0	0.0000	-0.0000	0.0000	0.0129	0.0000	0.0080	0.0000	-0.0000	-0.0000

Table 3 continued, part 5 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
60.00	0.00	0.00	0.0063	0.0000	0.0095	0.0024	-0.0000	0.0322	-0.0000	-0.0048	0.0000
60.00	0.00	0.00	0.0063	0.0016	0.0102	0.0023	-0.0016	0.0313	-0.0007	-0.0043	-0.0039
60.00	0.00	0.00	0.0059	0.0031	0.0122	0.0028	-0.0031	0.0295	-0.0013	-0.0037	-0.0073
60.00	0.00	0.00	0.0053	0.0041	0.0132	0.0034	-0.0041	0.0265	-0.0017	-0.0024	-0.0098
60.00	0.00	0.00	0.0047	0.0047	0.0189	0.0040	-0.0047	0.0228	-0.0019	-0.0008	-0.0112
60.00	0.00	0.00	0.0040	0.0047	0.0228	0.0047	-0.0047	0.0189	-0.0019	-0.0008	-0.0112
60.00	0.00	0.00	0.0034	0.0041	0.0265	0.0053	-0.0041	0.0152	-0.0017	-0.0024	-0.0098
60.00	0.00	0.00	0.0028	0.0031	0.0295	0.0059	-0.0031	0.0122	-0.0013	-0.0037	-0.0073
60.00	0.00	0.00	0.0023	0.0016	0.0315	0.0062	-0.0016	0.0102	-0.0007	-0.0043	-0.0039
60.00	0.00	0.00	0.0024	-0.0000	0.0322	0.0063	-0.0000	0.0095	-0.0000	-0.0048	0.0000
60.00	0.00	0.00	0.0038	0.0000	0.0388	0.0024	-0.0000	0.0320	-0.0000	-0.0043	0.0000
60.00	0.00	0.00	0.0037	0.0015	0.0094	0.0023	-0.0016	0.0314	-0.0006	-0.0043	0.0037
60.00	0.00	0.00	0.0053	0.0028	0.0112	0.0028	-0.0031	0.0294	-0.0012	-0.0035	-0.0069
60.00	0.00	0.00	0.0049	0.0037	0.0139	0.0033	-0.0041	0.0264	-0.0016	-0.0023	-0.0093
60.00	0.00	0.00	0.0043	0.0043	0.0172	0.0040	-0.0047	0.0227	-0.0018	-0.0008	-0.0106
60.00	0.00	0.00	0.0037	0.0042	0.0208	0.0047	-0.0047	0.0187	-0.0018	-0.0008	-0.0106
60.00	0.00	0.00	0.0031	0.0037	0.0241	0.0053	-0.0041	0.0150	-0.0016	-0.0023	-0.0093
60.00	0.00	0.00	0.0026	0.0028	0.0269	0.0058	-0.0031	0.0120	-0.0012	-0.0035	-0.0069
60.00	0.00	0.00	0.0023	0.0015	0.0286	0.0062	-0.0016	0.0101	-0.0006	-0.0043	-0.0037
60.00	0.00	0.00	0.0022	-0.0000	0.0293	0.0063	-0.0000	0.0094	-0.0000	-0.0048	0.0000
60.00	0.00	0.00	0.0043	0.0000	0.0368	0.0023	-0.0000	0.0316	-0.0000	-0.0043	0.0000
60.00	0.00	0.00	0.0042	0.0011	0.0072	0.0024	-0.0016	0.0309	-0.0006	-0.0043	0.0037
60.00	0.00	0.00	0.0040	0.0021	0.0086	0.0027	-0.0031	0.0289	-0.0010	-0.0030	-0.0060
60.00	0.00	0.00	0.0037	0.0028	0.0106	0.0033	-0.0041	0.0259	-0.0014	-0.0019	-0.0080
60.00	0.00	0.00	0.0032	0.0031	0.0130	0.0039	-0.0047	0.0222	-0.0016	-0.0007	-0.0091
60.00	0.00	0.00	0.0028	0.0031	0.0137	0.0046	-0.0047	0.0183	-0.0016	-0.0007	-0.0091
60.00	0.00	0.00	0.0023	0.0027	0.0181	0.0052	-0.0041	0.0146	-0.0014	-0.0020	-0.0090
60.00	0.00	0.00	0.0020	0.0020	0.0201	0.0057	-0.0031	0.0116	-0.0010	-0.0030	-0.0059
60.00	0.00	0.00	0.0018	0.0011	0.0214	0.0061	-0.0016	0.0097	-0.0003	-0.0037	-0.0031
60.00	0.00	0.00	0.0017	-0.0000	0.0219	0.0062	-0.0000	0.0090	-0.0000	-0.0048	0.0000
60.00	0.00	0.00	0.0026	0.0000	0.0243	0.0021	-0.0000	0.0311	-0.0000	-0.0043	0.0000
60.00	0.00	0.00	0.0026	0.0006	0.0043	0.0023	-0.0016	0.0304	-0.0004	-0.0028	0.0023
60.00	0.00	0.00	0.0024	0.0012	0.0053	0.0026	-0.0031	0.0284	-0.0008	-0.0023	-0.0046
60.00	0.00	0.00	0.0022	0.0016	0.0063	0.0031	-0.0041	0.0253	-0.0011	-0.0013	-0.0062
60.00	0.00	0.00	0.0020	0.0019	0.0080	0.0038	-0.0047	0.0216	-0.0012	-0.0003	-0.0070
60.00	0.00	0.00	0.0017	0.0018	0.0093	0.0043	-0.0047	0.0177	-0.0012	-0.0003	-0.0070
60.00	0.00	0.00	0.0014	0.0016	0.0110	0.0051	-0.0041	0.0140	-0.0011	-0.0013	-0.0061
60.00	0.00	0.00	0.0012	0.0012	0.0122	0.0056	-0.0030	0.0111	-0.0008	-0.0023	-0.0043
60.00	0.00	0.00	0.0011	0.0006	0.0129	0.0060	-0.0016	0.0091	-0.0004	-0.0028	-0.0024
60.00	0.00	0.00	0.0011	0.0000	0.0132	0.0061	-0.0000	0.0083	-0.0000	-0.0030	0.0000
60.00	0.00	0.00	0.0012	0.0000	0.0020	0.0020	-0.0000	0.0303	-0.0000	-0.0020	0.0000
60.00	0.00	0.00	0.0012	0.0003	0.0021	0.0021	-0.0016	0.0298	-0.0003	-0.0019	-0.0016
60.00	0.00	0.00	0.0011	0.0003	0.0023	0.0023	-0.0031	0.0278	-0.0003	-0.0013	-0.0031
60.00	0.00	0.00	0.0010	0.0007	0.0030	0.0030	-0.0042	0.0248	-0.0007	-0.0010	-0.0042
60.00	0.00	0.00	0.0009	0.0008	0.0037	0.0037	-0.0047	0.0211	-0.0008	-0.0003	-0.0047
60.00	0.00	0.00	0.0008	0.0008	0.0044	0.0044	-0.0047	0.0171	-0.0008	-0.0004	-0.0047
60.00	0.00	0.00	0.0007	0.0007	0.0050	0.0050	-0.0041	0.0135	-0.0007	-0.0010	-0.0041
60.00	0.00	0.00	0.0006	0.0003	0.0053	0.0053	-0.0030	0.0103	-0.0003	-0.0013	-0.0030
60.00	0.00	0.00	0.0005	0.0003	0.0058	0.0058	-0.0016	0.0086	-0.0000	-0.0019	-0.0016
60.00	0.00	0.00	0.0005	0.0000	0.0060	0.0060	-0.0000	0.0080	-0.0000	-0.0020	0.0000
60.00	0.00	0.00	0.0003	0.0000	0.0063	0.0063	-0.0000	0.0072	-0.0000	-0.0020	0.0000
60.00	0.00	0.00	0.0003	0.0001	0.0066	0.0021	-0.0017	0.0293	-0.0001	-0.0003	-0.0008
60.00	0.00	0.00	0.0003	0.0001	0.0066	0.0024	-0.0031	0.0274	-0.0003	-0.0003	-0.0013
60.00	0.00	0.00	0.0003	0.0002	0.0068	0.0030	-0.0042	0.0244	-0.0004	-0.0003	-0.0023
60.00	0.00	0.00	0.0002	0.0002	0.0069	0.0036	-0.0047	0.0207	-0.0004	-0.0003	-0.0023
60.00	0.00	0.00	0.0002	0.0002	0.0071	0.0043	-0.0047	0.0166	-0.0004	-0.0003	-0.0023
60.00	0.00	0.00	0.0001	0.0002	0.0072	0.0049	-0.0041	0.0131	-0.0004	-0.0003	-0.0020
60.00	0.00	0.00	0.0001	0.0001	0.0074	0.0054	-0.0030	0.0102	-0.0003	-0.0003	-0.0013
60.00	0.00	0.00	0.0001	0.0001	0.0075	0.0058	-0.0016	0.0083	-0.0001	-0.0003	-0.0008
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0059	-0.0000	0.0076	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0070	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0063	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0056	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0049	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0042	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0035	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0028	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0021	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0014	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0007	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0.00	0.00	0.0000	0.0000	0.0075	0.0060	-0.0000	0.0000	-0.0000	-0.0010	0.0000
60.00	0										

Table 3 continued, part 6 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$									
73	0	0	0	0016	0	0000	0	0092	0	0026	-0	0000	0	0318	-0	0000	-0	0024	0	0000
73	0	0	0	0013	0	0008	0	0098	0	0006	-0	0008	0	0311	-0	0002	-0	0022	0	0039
73	0	0	0	0015	0	0015	0	0118	0	0007	-0	0015	0	0291	-0	0003	-0	0018	-0	0073
73	0	0	0	0013	0	0021	0	0148	0	0004	-0	0021	0	0261	-0	0004	-0	0012	-0	0098
73	0	0	0	0012	0	0023	0	0185	0	0010	-0	0023	0	0224	-0	0005	-0	0004	-0	0111
73	0	0	0	0010	0	0023	0	0224	0	0012	-0	0023	0	0185	-0	0005	-0	0004	-0	0111
73	0	0	0	0009	0	0021	0	0261	0	0013	-0	0021	0	0148	-0	0004	-0	0012	-0	0098
73	0	0	0	0007	0	0015	0	0291	0	0015	-0	0015	0	0118	-0	0003	-0	0018	-0	0073
73	0	0	0	0006	0	0008	0	0311	0	0015	-0	0008	0	0098	-0	0002	-0	0022	-0	0333
73	0	0	0	0006	-0	0000	0	0318	0	0016	-0	0000	0	0092	-0	0000	-0	0024	0	0000
73	0	0	0	0014	0	0000	0	0084	0	0006	-0	0000	0	0316	-0	0000	-0	0023	0	0000
73	0	0	0	0014	0	0007	0	0090	0	0006	-0	0008	0	0309	-0	0002	-0	0021	-0	0037
73	0	0	0	0013	0	0014	0	0108	0	0007	-0	0015	0	0290	-0	0003	-0	0017	-0	0069
73	0	0	0	0012	0	0019	0	0135	0	0008	-0	0021	0	0239	-0	0004	-0	0011	-0	0293
73	0	0	0	0011	0	0021	0	0169	0	0010	-0	0023	0	0223	-0	0005	-0	0004	-0	0106
73	0	0	0	0009	0	0021	0	0204	0	0012	-0	0023	0	0183	-0	0005	-0	0004	-0	0106
73	0	0	0	0008	0	0019	0	0238	0	0013	-0	0020	0	0146	-0	0004	-0	0011	-0	0093
73	0	0	0	0007	0	0014	0	0265	0	0015	-0	0015	0	0116	-0	0003	-0	0017	-0	0069
73	0	0	0	0006	0	0007	0	0282	0	0015	-0	0008	0	0097	-0	0002	-0	0021	-0	0037
73	0	0	0	0006	-0	0000	0	0289	0	0014	-0	0000	0	0090	-0	0000	-0	0023	0	0000
73	0	0	0	0011	0	0000	0	0065	0	0006	-0	0000	0	0312	-0	0000	-0	0019	0	0000
73	0	0	0	0011	0	0005	0	0070	0	0006	-0	0008	0	0305	-0	0001	-0	0018	-0	0032
73	0	0	0	0010	0	0010	0	0083	0	0007	-0	0015	0	0283	-0	0003	-0	0013	-0	0060
73	0	0	0	0009	0	0014	0	0103	0	0008	-0	0021	0	0235	-0	0003	-0	0010	-0	0080
73	0	0	0	0008	0	0016	0	0128	0	0010	-0	0023	0	0218	-0	0004	-0	0003	-0	0091
73	0	0	0	0007	0	0016	0	0154	0	0011	-0	0023	0	0179	-0	0004	-0	0003	-0	0091
73	0	0	0	0006	0	0014	0	0178	0	0013	-0	0020	0	0142	-0	0003	-0	0010	-0	0080
73	0	0	0	0005	0	0010	0	0198	0	0014	-0	0015	0	0112	-0	0003	-0	0015	-0	0039
73	0	0	0	0005	-0	0000	0	0211	0	0015	-0	0008	0	0093	-0	0001	-0	0018	-0	0031
73	0	0	0	0004	-0	0000	0	0216	0	0015	-0	0000	0	0086	-0	0000	-0	0019	0	0000
73	0	0	0	0007	0	0000	0	0041	0	0005	-0	0000	0	0307	-0	0000	-0	0015	0	0000
73	0	0	0	0006	0	0003	0	0044	0	0006	-0	0008	0	0300	-0	0001	-0	0014	-0	0025
73	0	0	0	0006	0	0006	0	0052	0	0007	-0	0015	0	0280	-0	0002	-0	0011	-0	0046
73	0	0	0	0006	0	0008	0	0064	0	0008	-0	0021	0	0249	-0	0003	-0	0007	-0	0062
73	0	0	0	0005	0	0009	0	0078	0	0010	-0	0023	0	0212	-0	0003	-0	0002	-0	0070
73	0	0	0	0004	0	0009	0	0094	0	0011	-0	0023	0	0173	-0	0003	-0	0003	-0	0070
73	0	0	0	0004	0	0008	0	0108	0	0013	-0	0020	0	0136	-0	0003	-0	0008	-0	0061
73	0	0	0	0003	0	0006	0	0120	0	0014	-0	0015	0	0107	-0	0002	-0	0011	-0	0045
73	0	0	0	0003	0	0003	0	0127	0	0015	-0	0008	0	0068	-0	0001	-0	0014	-0	0024
73	0	0	0	0003	-0	0000	0	0130	0	0015	-0	0000	0	0081	-0	0000	-0	0015	0	0000
73	0	0	0	0003	0	0000	0	0019	0	0005	-0	0000	0	0302	-0	0000	-0	0010	0	0000
73	0	0	0	0003	0	0001	0	0021	0	0006	-0	0008	0	0295	-0	0001	-0	0009	-0	0017
73	0	0	0	0003	0	0003	0	0024	0	0006	-0	0015	0	0274	-0	0001	-0	0008	-0	0031
73	0	0	0	0003	0	0004	0	0030	0	0008	-0	0021	0	0244	-0	0002	-0	0005	-0	0042
73	0	0	0	0002	0	0004	0	0036	0	0009	-0	0023	0	0207	-0	0002	-0	0002	-0	0047
73	0	0	0	0002	0	0004	0	0043	0	0011	-0	0023	0	0168	-0	0002	-0	0002	-0	0047
73	0	0	0	0002	0	0004	0	0049	0	0012	-0	0020	0	0131	-0	0002	-0	0005	-0	0041
73	0	0	0	0001	0	0003	0	0054	0	0014	-0	0015	0	0102	-0	0001	-0	0008	-0	0030
73	0	0	0	0001	0	0001	0	0058	0	0015	-0	0008	0	0033	-0	0001	-0	0009	-0	0016
73	0	0	0	0001	-0	0000	0	0059	0	0015	-0	0000	0	0076	-0	0000	-0	0010	0	0000
73	0	0	0	0001	0	0000	0	0005	0	0005	-0	0000	0	0098	-0	0000	-0	0005	0	0000
73	0	0	0	0001	0	0000	0	0005	0	0005	-0	0008	0	0291	-0	0000	-0	0005	-0	0008
73	0	0	0	0001	0	0001	0	0006	0	0006	-0	0015	0	0271	-0	0001	-0	0005	-0	0015
73	0	0	0	0001	0	0001	0	0007	0	0007	-0	0021	0	0240	-0	0001	-0	0002	-0	0021
73	0	0	0	0001	0	0001	0	0009	0	0009	-0	0023	0	0203	-0	0001	-0	0001	-0	0023
73	0	0	0	0000	0	0001	0	0011	0	0011	-0	0023	0	0127	-0	0001	-0	0001	-0	0023
73	0	0	0	0000	0	0001	0	0012	0	0012	-0	0020	0	0127	-0	0001	-0	0003	-0	0020
73	0	0	0	0000	0	0001	0	0014	0	0014	-0	0008	0	0098	-0	0001	-0	0004	-0	0015
73	0	0	0	0000	0	0000	0	0014	0	0014	-0	0000	0	0079	-0	0000	-0	0005	-0	0008
73	0	0	0	0000	-0	0000	0	0015	0	0015	-0	0000	0	0073	-0	0000	-0	0005	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0005	-0	0000	0	0297	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0005	-0	0008	0	0290	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0006	-0	0015	0	0249	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0007	-0	0021	0	0239	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0009	-0	0023	0	0201	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0011	-0	0023	0	0162	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0012	-0	0020	0	0126	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0013	-0	0015	0	0097	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	0	0000	0	0000	0	0014	-0	0008	0	0078	-0	0000	-0	0000	-0	0000
73	0	0	0	0000	-0	0000	0	0000	0	0015	-0	0000	0	0072	-0	0000	-0	0000	-0	0000



Table 3 continued, part 7 of 7.

[illegible]



TABLE 4. PARAMETERS  $\sigma_1$ ,  $1 = 1, 2, \dots, 9$ , NORMALIZED TO  $\lambda^2$   
FOR SCATTERING FROM A  $3/2$ -WAVELENGTH DIPOLE  
( $L = 3\lambda/2$ ). ANGLES  $\theta_1$ ,  $\theta_2$ , AND  $\beta_\phi$  SHOWN IN DEGREES.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
0	0	0	0.1547	0.0000	0.0516	0.0516	-0.0000	0.1547	-0.0000	-0.0516	0.0000
0	0	10	0.1516	0.0176	0.0547	0.0547	-0.0176	0.1516	0.0176	-0.0485	0.0176
0	0	20	0.1427	0.0332	0.0636	0.0636	-0.0332	0.1427	0.0332	-0.0393	0.0332
0	0	30	0.1289	0.0447	0.0774	0.0774	-0.0447	0.1289	0.0447	-0.0298	0.0447
0	0	40	0.1121	0.0508	0.0942	0.0942	-0.0508	0.1121	0.0508	-0.0200	0.0508
0	0	50	0.0942	0.0447	0.1121	0.1121	-0.0447	0.0942	0.0447	-0.0090	0.0447
0	0	60	0.0774	0.0332	0.1289	0.1289	-0.0332	0.0774	0.0332	0.0000	0.0332
0	0	70	0.0636	0.0176	0.1427	0.1427	-0.0176	0.0636	0.0176	0.0090	0.0176
0	0	80	0.0547	0.0000	0.1516	0.1516	0.0000	0.0547	0.0000	0.0176	0.0000
0	0	90	0.0485	0.0176	0.1547	0.1547	0.0176	0.0485	0.0176	0.0298	0.0176
0	10	0	0.1406	0.0000	0.0474	0.0474	-0.0000	0.1406	0.0000	-0.0474	0.0000
0	10	10	0.1378	0.0159	0.0502	0.0502	-0.0159	0.1378	0.0159	-0.0461	0.0159
0	10	20	0.1247	0.0300	0.0583	0.0583	-0.0300	0.1247	0.0300	-0.0376	0.0300
0	10	30	0.1121	0.0404	0.0707	0.0707	-0.0404	0.1121	0.0404	-0.0283	0.0404
0	10	40	0.1021	0.0459	0.0859	0.0859	-0.0459	0.1021	0.0459	-0.0183	0.0459
0	10	50	0.0859	0.0459	0.1021	0.1021	-0.0459	0.0859	0.0459	-0.0076	0.0459
0	10	60	0.0707	0.0404	0.1121	0.1121	-0.0404	0.0707	0.0404	0.0000	0.0404
0	10	70	0.0583	0.0300	0.1247	0.1247	-0.0300	0.0583	0.0300	0.0076	0.0300
0	10	80	0.0502	0.0159	0.1378	0.1378	-0.0159	0.0502	0.0159	0.0183	0.0159
0	10	90	0.0474	0.0000	0.1406	0.1406	0.0000	0.0474	0.0000	0.0283	0.0000
0	20	0	0.1308	0.0000	0.0386	0.0386	-0.0000	0.1308	0.0000	-0.0386	0.0000
0	20	10	0.1289	0.0118	0.0437	0.0437	-0.0118	0.1289	0.0118	-0.0363	0.0118
0	20	20	0.1247	0.0221	0.0508	0.0508	-0.0221	0.1247	0.0221	-0.0323	0.0221
0	20	30	0.1183	0.0333	0.0583	0.0583	-0.0333	0.1183	0.0333	-0.0271	0.0333
0	20	40	0.1106	0.0444	0.0668	0.0668	-0.0444	0.1106	0.0444	-0.0211	0.0444
0	20	50	0.1019	0.0544	0.0774	0.0774	-0.0544	0.1019	0.0544	-0.0144	0.0544
0	20	60	0.0921	0.0621	0.0880	0.0880	-0.0621	0.0921	0.0621	-0.0076	0.0621
0	20	70	0.0819	0.0672	0.0972	0.0972	-0.0672	0.0819	0.0672	0.0000	0.0672
0	20	80	0.0707	0.0699	0.1052	0.1052	-0.0699	0.0707	0.0699	0.0076	0.0699
0	20	90	0.0583	0.0699	0.1118	0.1118	-0.0699	0.0583	0.0699	0.0144	0.0699
0	30	0	0.1183	0.0000	0.0320	0.0320	-0.0000	0.1183	0.0000	-0.0320	0.0000
0	30	10	0.1164	0.0069	0.0342	0.0342	-0.0069	0.1164	0.0069	-0.0303	0.0069
0	30	20	0.1121	0.0131	0.0377	0.0377	-0.0131	0.1121	0.0131	-0.0271	0.0131
0	30	30	0.1052	0.0176	0.0431	0.0431	-0.0176	0.1052	0.0176	-0.0221	0.0176
0	30	40	0.0969	0.0200	0.0468	0.0468	-0.0200	0.0969	0.0200	-0.0166	0.0200
0	30	50	0.0876	0.0214	0.0497	0.0497	-0.0214	0.0876	0.0214	-0.0111	0.0214
0	30	60	0.0774	0.0221	0.0516	0.0516	-0.0221	0.0774	0.0221	-0.0056	0.0221
0	30	70	0.0668	0.0214	0.0521	0.0521	-0.0214	0.0668	0.0214	0.0000	0.0214
0	30	80	0.0554	0.0199	0.0516	0.0516	-0.0199	0.0554	0.0199	0.0056	0.0199
0	30	90	0.0431	0.0176	0.0497	0.0497	-0.0176	0.0431	0.0176	0.0111	0.0176
0	40	0	0.1052	0.0000	0.0277	0.0277	-0.0000	0.1052	0.0000	-0.0277	0.0000
0	40	10	0.1033	0.0069	0.0297	0.0297	-0.0069	0.1033	0.0069	-0.0258	0.0069
0	40	20	0.1019	0.0131	0.0320	0.0320	-0.0131	0.1019	0.0131	-0.0221	0.0131
0	40	30	0.0969	0.0176	0.0342	0.0342	-0.0176	0.0969	0.0176	-0.0176	0.0176
0	40	40	0.0907	0.0200	0.0363	0.0363	-0.0200	0.0907	0.0200	-0.0121	0.0200
0	40	50	0.0833	0.0214	0.0377	0.0377	-0.0214	0.0833	0.0214	-0.0069	0.0214
0	40	60	0.0744	0.0221	0.0386	0.0386	-0.0221	0.0744	0.0221	0.0000	0.0221
0	40	70	0.0644	0.0214	0.0391	0.0391	-0.0214	0.0644	0.0214	0.0056	0.0214
0	40	80	0.0533	0.0199	0.0391	0.0391	-0.0199	0.0533	0.0199	0.0111	0.0199
0	40	90	0.0419	0.0176	0.0377	0.0377	-0.0176	0.0419	0.0176	0.0166	0.0176
0	50	0	0.0907	0.0000	0.0230	0.0230	-0.0000	0.0907	0.0000	-0.0230	0.0000
0	50	10	0.0888	0.0069	0.0242	0.0242	-0.0069	0.0888	0.0069	-0.0211	0.0069
0	50	20	0.0876	0.0131	0.0257	0.0257	-0.0131	0.0876	0.0131	-0.0176	0.0131
0	50	30	0.0833	0.0176	0.0277	0.0277	-0.0176	0.0833	0.0176	-0.0121	0.0176
0	50	40	0.0774	0.0200	0.0297	0.0297	-0.0200	0.0774	0.0200	-0.0069	0.0200
0	50	50	0.0707	0.0214	0.0308	0.0308	-0.0214	0.0707	0.0214	0.0000	0.0214
0	50	60	0.0621	0.0221	0.0313	0.0313	-0.0221	0.0621	0.0221	0.0056	0.0221
0	50	70	0.0521	0.0214	0.0313	0.0313	-0.0214	0.0521	0.0214	0.0111	0.0214
0	50	80	0.0419	0.0199	0.0308	0.0308	-0.0199	0.0419	0.0199	0.0166	0.0199
0	50	90	0.0308	0.0176	0.0297	0.0297	-0.0176	0.0308	0.0176	0.0211	0.0176
0	60	0	0.0819	0.0000	0.0183	0.0183	-0.0000	0.0819	0.0000	-0.0183	0.0000
0	60	10	0.0800	0.0069	0.0199	0.0199	-0.0069	0.0800	0.0069	-0.0166	0.0069
0	60	20	0.0774	0.0131	0.0214	0.0214	-0.0131	0.0774	0.0131	-0.0121	0.0131
0	60	30	0.0744	0.0176	0.0221	0.0221	-0.0176	0.0744	0.0176	-0.0069	0.0176
0	60	40	0.0699	0.0200	0.0221	0.0221	-0.0200	0.0699	0.0200	0.0000	0.0200
0	60	50	0.0644	0.0214	0.0221	0.0221	-0.0214	0.0644	0.0214	0.0056	0.0214
0	60	60	0.0583	0.0221	0.0221	0.0221	-0.0221	0.0583	0.0221	0.0111	0.0221
0	60	70	0.0516	0.0214	0.0214	0.0214	-0.0214	0.0516	0.0214	0.0166	0.0214
0	60	80	0.0444	0.0199	0.0200	0.0200	-0.0199	0.0444	0.0199	0.0211	0.0199
0	60	90	0.0377	0.0176	0.0183	0.0183	-0.0176	0.0377	0.0176	0.0258	0.0176
0	70	0	0.0707	0.0000	0.0108	0.0108	-0.0000	0.0707	0.0000	-0.0108	0.0000
0	70	10	0.0688	0.0069	0.0121	0.0121	-0.0069	0.0688	0.0069	-0.0090	0.0069
0	70	20	0.0668	0.0131	0.0131	0.0131	-0.0131	0.0668	0.0131	-0.0033	0.0131
0	70	30	0.0644	0.0176	0.0131	0.0131	-0.0176	0.0644	0.0176	0.0000	0.0176
0	70	40	0.0607	0.0200	0.0121	0.0121	-0.0200	0.0607	0.0200	0.0033	0.0200
0	70	50	0.0554	0.0214	0.0108	0.0108	-0.0214	0.0554	0.0214	0.0069	0.0214
0	70	60	0.0497	0.0221	0.0090	0.0090	-0.0221	0.0497	0.0221	0.0111	0.0221
0	70	70	0.0431	0.0214	0.0076	0.0076	-0.0214	0.0431	0.0214	0.0166	0.0214
0	70	80	0.0363	0.0199	0.0056	0.0056	-0.0199	0.0363	0.0199	0.0211	0.0199
0	70	90	0.0297	0.0176	0.0033	0.0033	-0.0176	0.0297	0.0176	0.0258	0.0176
0	80	0	0.0607	0.0000	0.0029	0.0029	-0.0000	0.0607	0.0000	-0.0029	0.0000
0	80	10	0.0583	0.0069	0.0033	0.0033	-0.0069	0.0583	0.0069	-0.0019	0.0069
0	80	20	0.0554	0.0131	0.0033	0.0033	-0.0131	0.0554	0.0131	0.0000	0.0131
0	80	30	0.0516	0.0176	0.0033	0.0033	-0.0176	0.0516	0.0176	0.0033	0.0176
0	80	40	0.0474	0.0200	0.0033	0.0033	-0.0200	0.0474	0.0200	0.0069	0.0200
0	80	50	0.0431	0.0214	0.0033	0.0033	-0.0214	0.0431	0.0214	0.0111	0.0214
0	80	60	0.0386	0.0221	0.0033	0.0033	-0.0221	0.0386	0.0221	0.0166	0.0221
0	80	70	0.0333	0.0214	0.0029	0.0029	-0.0214	0.0333	0.0214	0.0211	0.0214
0	80	80	0.0277	0.0199	0.0019	0.0019	-0.0199	0.0277	0.0199	0.0258	0.0199
0	80	90	0.0221	0.0176	0.0000	0.0000	-0.0176	0.0221	0.0176	0.0300	0.0176
0	90	0	0.0516	0.0000	0.0000	0.0000	-0.0000	0.0516	0.0000	-0.0000	0.0000
0	90	10	0.0485	0.0176	0.0000	0.0000	-0.0176	0.0485	0.0176	0.0000	0.0176
0	90	20	0.0447	0.0332	0.0000	0.0000	-0.0332	0.0447	0.0332	0.0000	0.0332
0	90	30	0.0404	0.0447	0.0000	0.0000	-0.0447	0.0404	0.0447	0.0000	0.0447
0	90	40	0.0350	0.0508	0.0000	0.0000	-0.0508	0.0350	0.0508	0.0000	0.0508
0	90	50	0.0298	0.0447	0.0000	0.0000	-0.0447	0.0298	0.0447	0.0000	0.0447
0	90	60	0.0244	0.0332	0.0000	0.0000	-0.0332	0.0244	0.0332	0.0000	0.0332

Table 4 continued, part 2 of 7.

[illegible]

Table 4 continued, part 3 of 7.

$\theta_1$	$\theta_2$	$B_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$									
30	0	0	0	1032	0	0000	0	0487	0	0365	-0	0000	0	1518	-0	0000	-0	0421	0	0000
30	0	0	0	1032	0	0144	0	0518	0	0386	-0	0144	0	1487	0	0118	-0	0396	-0	0176
30	0	0	0	0972	0	0271	0	0607	0	0443	-0	0271	0	1397	0	0221	-0	0373	-0	0331
30	0	0	0	0880	0	0363	0	0744	0	0537	-0	0363	0	1260	0	0298	-0	0211	-0	0446
30	0	0	0	0768	0	0413	0	0913	0	0649	-0	0413	0	1092	0	0338	-0	0073	-0	0508
30	0	0	0	0649	0	0413	0	1092	0	0768	-0	0413	0	0913	0	0338	-0	0073	-0	0508
30	0	0	0	0537	0	0363	0	1260	0	0880	-0	0363	0	0744	0	0298	-0	0211	-0	0446
30	0	0	0	0443	0	0271	0	1397	0	0972	-0	0271	0	0607	0	0221	-0	0373	-0	0331
30	0	0	0	0386	0	0144	0	1487	0	1032	-0	0144	0	0518	0	0118	-0	0396	-0	0176
30	0	0	0	0363	-0	0000	0	1518	0	1032	-0	0000	0	0487	-0	0000	-0	0421	0	0000
30	0	0	0	0957	0	0000	0	0447	0	0359	-0	0000	0	1510	-0	0000	-0	0401	0	0000
30	0	0	0	0938	0	0130	0	0475	0	0380	-0	0144	0	1479	0	0112	-0	0377	-0	0168
30	0	0	0	0884	0	0243	0	0556	0	0440	-0	0271	0	1389	0	0210	-0	0307	-0	0315
30	0	0	0	0801	0	0330	0	0680	0	0531	-0	0363	0	1252	0	0283	-0	0200	-0	0425
30	0	0	0	0700	0	0373	0	0832	0	0644	-0	0413	0	1084	0	0322	-0	0069	-0	0483
30	0	0	0	0592	0	0373	0	0994	0	0763	-0	0413	0	0905	0	0322	-0	0070	-0	0483
30	0	0	0	0490	0	0330	0	1146	0	0875	-0	0363	0	0736	0	0283	-0	0200	-0	0424
30	0	0	0	0408	0	0243	0	1270	0	0966	-0	0271	0	0599	0	0210	-0	0307	-0	0315
30	0	0	0	0354	0	0130	0	1351	0	1026	-0	0144	0	0510	0	0112	-0	0376	-0	0168
30	0	0	0	0333	-0	0000	0	1379	0	1047	-0	0000	0	0479	-0	0000	-0	0401	0	0000
30	0	0	0	0316	0	0000	0	0345	0	0345	-0	0000	0	0300	-0	0000	-0	0345	0	0000
30	0	0	0	0272	0	0096	0	0363	0	0363	-0	0144	0	1358	0	0096	-0	0324	-0	0144
30	0	0	0	0262	0	0181	0	0425	0	0425	-0	0271	0	1368	0	0181	-0	0264	-0	0271
30	0	0	0	0201	0	0243	0	0517	0	0517	-0	0363	0	1231	0	0243	-0	0172	-0	0363
30	0	0	0	0126	0	0277	0	0629	0	0629	-0	0413	0	1063	0	0277	-0	0059	-0	0413
30	0	0	0	0447	0	0276	0	0748	0	0748	-0	0413	0	0884	0	0276	-0	0060	-0	0413
30	0	0	0	0372	0	0243	0	0860	0	0860	-0	0364	0	0716	0	0243	-0	0172	-0	0364
30	0	0	0	0311	0	0180	0	0952	0	0952	-0	0270	0	0579	0	0180	-0	0264	-0	0270
30	0	0	0	0272	0	0096	0	1011	0	1011	-0	0144	0	0490	0	0096	-0	0323	-0	0144
30	0	0	0	0258	-0	0000	0	1032	0	1032	-0	0000	0	0459	-0	0000	-0	0344	0	0000
30	0	0	0	0433	0	0000	0	1027	0	0325	-0	0000	0	1462	-0	0000	-0	0266	0	0000
30	0	0	0	0425	0	0057	0	0229	0	0346	-0	0144	0	1431	0	0074	-0	0250	-0	0111
30	0	0	0	0401	0	0107	0	0265	0	0406	-0	0271	0	1341	0	0139	-0	0203	-0	0209
30	0	0	0	0365	0	0144	0	0319	0	0498	-0	0363	0	1203	0	0188	-0	0132	-0	0282
30	0	0	0	0320	0	0163	0	0365	0	0610	-0	0413	0	1035	0	0213	-0	0046	-0	0320
30	0	0	0	0273	0	0163	0	0456	0	0729	-0	0414	0	0856	0	0213	-0	0046	-0	0319
30	0	0	0	0229	0	0143	0	0522	0	0841	-0	0364	0	0689	0	0187	-0	0133	-0	0281
30	0	0	0	0194	0	0106	0	0576	0	0932	-0	0270	0	0689	0	0187	-0	0133	-0	0281
30	0	0	0	0170	-0	0000	0	0611	0	0991	-0	0143	0	0462	-0	0074	-0	0249	-0	0111
30	0	0	0	0162	-0	0000	0	0623	0	1012	-0	0000	0	0432	-0	0000	-0	0265	0	0000
30	0	0	0	0196	0	0000	0	0102	0	0307	-0	0000	0	1436	-0	0000	-0	0178	-0	0000
30	0	0	0	0192	0	0029	0	0108	0	0328	-0	0144	0	1405	0	0030	-0	0167	-0	0074
30	0	0	0	0182	0	0047	0	0124	0	0388	-0	0271	0	1319	0	0093	-0	0136	-0	0140
30	0	0	0	0166	0	0064	0	0148	0	0480	-0	0363	0	1177	0	0123	-0	0088	-0	0188
30	0	0	0	0146	0	0072	0	0177	0	0592	-0	0414	0	1009	0	0142	-0	0030	-0	0214
30	0	0	0	0125	0	0072	0	0208	0	0711	-0	0413	0	0830	0	0142	-0	0031	-0	0213
30	0	0	0	0106	0	0063	0	0237	0	0823	-0	0363	0	0663	0	0123	-0	0069	-0	0187
30	0	0	0	0090	0	0047	0	0261	0	0913	-0	0269	0	0527	0	0093	-0	0136	-0	0139
30	0	0	0	0080	0	0025	0	0276	0	0972	-0	0143	0	0439	0	0049	-0	0166	-0	0074
30	0	0	0	0076	-0	0000	0	0282	0	0993	-0	0000	0	0408	-0	0000	-0	0177	0	0000
30	0	0	0	0049	0	0000	0	0026	0	0295	-0	0000	0	1417	-0	0000	-0	0088	0	0000
30	0	0	0	0048	0	0006	0	0028	0	0314	-0	0144	0	1386	0	0023	-0	0083	-0	0037
30	0	0	0	0045	0	0012	0	0032	0	0376	-0	0271	0	1276	0	0046	-0	0067	-0	0069
30	0	0	0	0041	0	0016	0	0037	0	0468	-0	0364	0	1158	0	0062	-0	0044	-0	0093
30	0	0	0	0037	0	0018	0	0045	0	0580	-0	0413	0	0990	0	0071	-0	0019	-0	0106
30	0	0	0	0032	0	0018	0	0052	0	0699	-0	0413	0	0812	0	0071	-0	0016	-0	0106
30	0	0	0	0027	0	0015	0	0059	0	0810	-0	0362	0	0645	0	0062	-0	0047	-0	0093
30	0	0	0	0023	0	0011	0	0065	0	0900	-0	0268	0	0510	0	0046	-0	0067	-0	0069
30	0	0	0	0020	0	0006	0	0069	0	0959	-0	0143	0	0421	0	0024	-0	0082	-0	0037
30	0	0	0	0020	-0	0000	0	0070	0	0979	-0	0000	0	0391	-0	0000	-0	0088	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0291	-0	0000	0	1410	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0311	-0	0144	0	1379	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0372	-0	0271	0	1289	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0463	-0	0364	0	1152	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0573	-0	0413	0	0984	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0694	-0	0412	0	0806	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0803	-0	0362	0	0639	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0895	-0	0268	0	0503	-0	0000	-0	0000	0	0000
30	0	0	0	0000	0	0000	0	0000	0	0954	-0	0143	0	0415	-0	0000	-0	0000	0	0000
30	0	0	0	0000	-0	0000	0	0000	0	0974	0	0000	0	0385	0	0000	-0	0000	-0	0000

Table 4 continued, part 4 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
44	0	0	0.0636	0.0000	0.0459	0.0230	-0.0000	0.1489	-0.0000	-0.0325	-0.0000
44	0	0	0.0623	0.0111	0.0490	0.0242	-0.0111	0.1458	-0.0069	-0.0305	-0.0176
44	0	0	0.0588	0.0209	0.0580	0.0277	-0.0209	0.1369	-0.0131	-0.0249	-0.0331
44	0	0	0.0534	0.0281	0.0717	0.0331	-0.0281	0.1232	-0.0176	-0.0162	-0.0446
44	0	0	0.0468	0.0320	0.0885	0.0397	-0.0320	0.1064	-0.0200	-0.0056	-0.0507
44	0	0	0.0397	0.0320	0.1064	0.0468	-0.0320	0.0885	-0.0200	0.0056	-0.0507
44	0	0	0.0331	0.0281	0.1232	0.0534	-0.0281	0.0717	-0.0176	0.0162	-0.0446
44	0	0	0.0277	0.0209	0.1369	0.0588	-0.0209	0.0580	-0.0131	0.0249	-0.0331
44	0	0	0.0242	0.0111	0.1458	0.0623	-0.0111	0.0490	-0.0069	0.0305	-0.0176
44	0	0	0.0230	-0.0000	0.1489	0.0636	-0.0000	0.0459	-0.0000	0.0325	-0.0000
44	0	0	0.0378	0.0000	0.0422	0.0226	-0.0000	0.1482	-0.0000	-0.0309	-0.0000
44	0	0	0.0367	0.0100	0.0450	0.0238	-0.0111	0.1451	-0.0066	-0.0270	-0.0168
44	0	0	0.0335	0.0189	0.0531	0.0274	-0.0209	0.1361	-0.0124	-0.0237	-0.0315
44	0	0	0.0486	0.0254	0.0555	0.0328	-0.0281	0.1224	-0.0167	-0.0154	-0.0424
44	0	0	0.0426	0.0289	0.0807	0.0394	-0.0320	0.1036	-0.0190	-0.0053	-0.0482
44	0	0	0.0362	0.0289	0.0807	0.0469	-0.0320	0.0877	-0.0190	0.0053	-0.0482
44	0	0	0.0302	0.0254	0.1121	0.0531	-0.0281	0.0709	-0.0167	0.0154	-0.0424
44	0	0	0.0234	0.0189	0.1243	0.0588	-0.0209	0.0572	-0.0124	0.0236	-0.0315
44	0	0	0.0222	0.0100	0.1325	0.0620	-0.0111	0.0483	-0.0066	0.0270	-0.0167
44	0	0	0.0211	-0.0000	0.1353	0.0632	-0.0000	0.0452	-0.0000	0.0309	-0.0000
44	0	0	0.0433	0.0000	0.0323	0.0217	-0.0000	0.1462	-0.0000	-0.0286	-0.0000
44	0	0	0.0429	0.0074	0.0346	0.0224	-0.0111	0.1431	-0.0057	-0.0270	-0.0144
44	0	0	0.0401	0.0139	0.0406	0.0263	-0.0209	0.1341	-0.0107	-0.0203	-0.0271
44	0	0	0.0369	0.0188	0.0498	0.0319	-0.0281	0.1203	-0.0144	-0.0132	-0.0365
44	0	0	0.0320	0.0213	0.0610	0.0389	-0.0320	0.1035	-0.0163	-0.0046	-0.0415
44	0	0	0.0273	0.0213	0.0729	0.0456	-0.0319	0.0856	-0.0163	0.0046	-0.0414
44	0	0	0.0229	0.0187	0.0841	0.0522	-0.0281	0.0689	-0.0143	0.0133	-0.0364
44	0	0	0.0194	0.0139	0.0932	0.0576	-0.0208	0.0552	-0.0106	0.0203	-0.0270
44	0	0	0.0170	0.0074	0.0991	0.0611	-0.0111	0.0463	-0.0057	0.0249	-0.0143
44	0	0	0.0166	-0.0000	0.1012	0.0623	-0.0000	0.0432	-0.0000	0.0265	-0.0000
44	0	0	0.0266	0.0000	0.0203	0.0203	-0.0000	0.1436	-0.0000	-0.0203	-0.0000
44	0	0	0.0257	0.0044	0.0217	0.0217	-0.0112	0.1405	-0.0044	-0.0143	-0.0112
44	0	0	0.0243	0.0083	0.0253	0.0253	-0.0209	0.1314	-0.0083	-0.0157	-0.0209
44	0	0	0.0221	0.0111	0.0308	0.0308	-0.0282	0.1176	-0.0111	-0.0102	-0.0282
44	0	0	0.0193	0.0126	0.0374	0.0374	-0.0320	0.1008	-0.0126	-0.0035	-0.0320
44	0	0	0.0167	0.0126	0.0444	0.0444	-0.0319	0.0829	-0.0126	0.0036	-0.0319
44	0	0	0.0141	0.0110	0.0510	0.0510	-0.0290	0.0642	-0.0110	0.0103	-0.0290
44	0	0	0.0120	0.0082	0.0564	0.0564	-0.0207	0.0526	-0.0082	0.0156	-0.0207
44	0	0	0.0107	0.0043	0.0599	0.0599	-0.0110	0.0438	-0.0043	0.0191	-0.0110
44	0	0	0.0102	-0.0000	0.0611	0.0611	-0.0000	0.0407	-0.0000	0.0204	-0.0000
44	0	0	0.0119	0.0000	0.0557	0.0557	-0.0000	0.0411	-0.0000	-0.0157	-0.0000
44	0	0	0.0116	0.0020	0.0502	0.0502	-0.0112	0.0379	-0.0039	-0.0124	-0.0075
44	0	0	0.0110	0.0037	0.0418	0.0418	-0.0210	0.0289	-0.0053	-0.0103	-0.0140
44	0	0	0.0101	0.0049	0.0343	0.0343	-0.0282	0.0207	-0.0074	-0.0068	-0.0188
44	0	0	0.0089	0.0036	0.0271	0.0271	-0.0319	0.0151	-0.0051	-0.0023	-0.0213
44	0	0	0.0077	0.0033	0.0220	0.0220	-0.0318	0.0084	-0.0034	-0.0024	-0.0213
44	0	0	0.0063	0.0049	0.0149	0.0149	-0.0279	0.0037	-0.0023	-0.0017	-0.0186
44	0	0	0.0056	0.0036	0.0097	0.0097	-0.0207	0.0050	-0.0034	-0.0014	-0.0138
44	0	0	0.0050	0.0019	0.0062	0.0062	-0.0110	0.0041	-0.0023	-0.0009	-0.0073
44	0	0	0.0038	0.0000	0.0027	0.0027	-0.0000	0.0038	-0.0000	0.0012	-0.0000
44	0	0	0.0030	0.0000	0.0025	0.0025	-0.0000	0.0030	-0.0000	0.0008	-0.0000
44	0	0	0.0027	0.0003	0.0020	0.0020	-0.0112	0.0013	-0.0003	0.0004	-0.0037
44	0	0	0.0023	0.0009	0.0015	0.0015	-0.0210	0.0000	-0.0000	0.0000	-0.0070
44	0	0	0.0021	0.0012	0.0010	0.0010	-0.0282	0.0000	-0.0000	0.0000	-0.0094
44	0	0	0.0019	0.0014	0.0007	0.0007	-0.0318	0.0000	-0.0000	0.0000	-0.0106
44	0	0	0.0017	0.0012	0.0005	0.0005	-0.0278	0.0000	-0.0000	0.0000	-0.0092
44	0	0	0.0014	0.0009	0.0004	0.0004	-0.0206	0.0000	-0.0000	0.0000	-0.0068
44	0	0	0.0013	0.0005	0.0003	0.0003	-0.0109	0.0000	-0.0000	0.0000	-0.0036
44	0	0	0.0012	0.0000	0.0002	0.0002	-0.0000	0.0000	-0.0000	0.0000	-0.0020
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000
44	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0000	-0.0000	0.0000	-0.0000

Table 4 continued, part 5 of 7.

$\theta_1$	$\theta_2$	$\theta_3$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
60.0	0.0	0.0	0.0288	0.0000	0.0433	0.0108	-0.0000	0.1462	-0.0000	-0.0217	0.0000
60.0	0.0	0.0	0.0282	0.0074	0.0464	0.0114	-0.0074	0.1431	0.0031	-0.0204	-0.0176
60.0	0.0	0.0	0.0267	0.0139	0.0534	0.0129	-0.0139	0.1241	0.0038	-0.0166	-0.0331
60.0	0.0	0.0	0.0243	0.0188	0.0591	0.0153	-0.0188	0.1203	0.0078	-0.0103	-0.0443
60.0	0.0	0.0	0.0214	0.0213	0.0658	0.0182	-0.0213	0.1037	0.0083	-0.0003	-0.0506
60.0	0.0	0.0	0.0182	0.0213	0.0707	0.0214	-0.0213	0.0858	0.0088	0.0003	-0.0503
60.0	0.0	0.0	0.0153	0.0188	0.0705	0.0243	-0.0188	0.0691	0.0078	0.0103	-0.0443
60.0	0.0	0.0	0.0129	0.0139	0.0741	0.0267	-0.0139	0.0534	0.0058	0.0165	-0.0331
60.0	0.0	0.0	0.0114	0.0074	0.0741	0.0282	-0.0074	0.0464	0.0031	0.0204	-0.0176
60.0	0.0	0.0	0.0108	0.0000	0.0741	0.0288	0.0000	0.0433	-0.0000	0.0217	0.0000
60.0	0.0	0.0	0.0082	0.0000	0.0798	0.0107	-0.0000	0.1455	-0.0000	-0.0206	0.0000
60.0	0.0	0.0	0.0067	0.0067	0.0741	0.0112	-0.0074	0.1424	0.0029	-0.0174	-0.0167
60.0	0.0	0.0	0.0243	0.0126	0.0507	0.0128	-0.0139	0.1334	0.0055	-0.0153	-0.0315
60.0	0.0	0.0	0.0221	0.0170	0.0631	0.0152	-0.0188	0.1197	0.0074	-0.0103	-0.0424
60.0	0.0	0.0	0.0194	0.0193	0.0783	0.0181	-0.0213	0.1029	0.0084	-0.0026	-0.0482
60.0	0.0	0.0	0.0166	0.0193	0.0945	0.0212	-0.0213	0.0851	0.0084	0.0036	-0.0481
60.0	0.0	0.0	0.0140	0.0170	0.1096	0.0241	-0.0188	0.0683	0.0074	0.0103	-0.0423
60.0	0.0	0.0	0.0118	0.0126	0.1220	0.0265	-0.0139	0.0545	0.0055	0.0153	-0.0314
60.0	0.0	0.0	0.0104	0.0067	0.1300	0.0281	-0.0074	0.0457	0.0029	0.0194	-0.0167
60.0	0.0	0.0	0.0099	0.0000	0.1328	0.0286	0.0000	0.0426	-0.0000	0.0206	0.0000
60.0	0.0	0.0	0.0196	0.0000	0.0307	0.0102	-0.0000	0.1436	-0.0000	-0.0178	0.0000
60.0	0.0	0.0	0.0193	0.0000	0.0325	0.0108	-0.0074	0.1403	0.0025	-0.0167	-0.0144
60.0	0.0	0.0	0.0182	0.0000	0.0388	0.0124	-0.0140	0.1315	0.0047	-0.0136	-0.0271
60.0	0.0	0.0	0.0166	0.0126	0.0480	0.0148	-0.0188	0.1177	0.0064	-0.0083	-0.0363
60.0	0.0	0.0	0.0145	0.0126	0.0599	0.0177	-0.0213	0.1009	0.0074	-0.0030	-0.0414
60.0	0.0	0.0	0.0122	0.0126	0.0711	0.0203	-0.0213	0.0820	0.0074	0.0031	-0.0413
60.0	0.0	0.0	0.0106	0.0126	0.0821	0.0237	-0.0187	0.0653	0.0064	0.0059	-0.0363
60.0	0.0	0.0	0.0088	0.0099	0.0945	0.0261	-0.0139	0.0527	0.0047	0.0136	-0.0269
60.0	0.0	0.0	0.0079	0.0079	0.1096	0.0274	-0.0074	0.0409	0.0029	0.0177	-0.0145
60.0	0.0	0.0	0.0069	0.0000	0.1194	0.0283	0.0000	0.0309	-0.0000	0.0207	0.0000
60.0	0.0	0.0	0.0060	0.0000	0.1283	0.0287	0.0000	0.0211	-0.0000	0.0237	0.0000
60.0	0.0	0.0	0.0050	0.0000	0.1369	0.0102	-0.0140	0.1279	0.0020	-0.0127	-0.0112
60.0	0.0	0.0	0.0041	0.0000	0.1455	0.0118	-0.0188	0.1289	0.0037	-0.0103	-0.0210
60.0	0.0	0.0	0.0033	0.0000	0.1541	0.0133	-0.0188	0.1181	0.0046	-0.0068	-0.0284
60.0	0.0	0.0	0.0024	0.0000	0.1626	0.0148	-0.0213	0.0982	0.0053	-0.0023	-0.0318
60.0	0.0	0.0	0.0015	0.0000	0.1711	0.0164	-0.0188	0.0804	0.0053	0.0024	-0.0318
60.0	0.0	0.0	0.0007	0.0000	0.1796	0.0179	-0.0188	0.0637	0.0047	0.0069	-0.0279
60.0	0.0	0.0	0.0000	0.0000	0.1880	0.0193	-0.0139	0.0502	0.0036	0.0104	-0.0207
60.0	0.0	0.0	0.0000	0.0000	0.1964	0.0207	-0.0074	0.0414	0.0019	0.0128	-0.0110
60.0	0.0	0.0	0.0000	0.0000	0.2048	0.0221	0.0000	0.0384	-0.0000	0.0136	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.2132	0.0235	0.0000	0.0354	-0.0000	0.0092	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.2216	0.0249	0.0073	0.0324	-0.0013	-0.0086	-0.0075
60.0	0.0	0.0	0.0000	0.0000	0.2300	0.0263	0.0140	0.0294	-0.0025	-0.0070	-0.0140
60.0	0.0	0.0	0.0000	0.0000	0.2384	0.0277	0.0188	0.0264	-0.0033	-0.0043	-0.0188
60.0	0.0	0.0	0.0000	0.0000	0.2468	0.0291	0.0213	0.0234	-0.0037	-0.0015	-0.0213
60.0	0.0	0.0	0.0000	0.0000	0.2552	0.0305	0.0212	0.0204	-0.0037	0.0016	-0.0212
60.0	0.0	0.0	0.0000	0.0000	0.2636	0.0319	0.0186	0.0174	-0.0032	0.0046	-0.0186
60.0	0.0	0.0	0.0000	0.0000	0.2720	0.0333	0.0137	0.0144	-0.0024	0.0070	-0.0137
60.0	0.0	0.0	0.0000	0.0000	0.2804	0.0347	0.0073	0.0111	-0.0013	0.0093	-0.0073
60.0	0.0	0.0	0.0000	0.0000	0.2888	0.0361	0.0000	0.0078	-0.0000	0.0090	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.2972	0.0375	0.0000	0.0044	-0.0000	0.0046	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.3056	0.0389	0.0075	0.0009	-0.0007	-0.0043	-0.0037
60.0	0.0	0.0	0.0000	0.0000	0.3140	0.0403	0.0141	0.0000	-0.0012	-0.0035	-0.0070
60.0	0.0	0.0	0.0000	0.0000	0.3224	0.0417	0.0188	0.0000	-0.0016	-0.0022	-0.0094
60.0	0.0	0.0	0.0000	0.0000	0.3308	0.0431	0.0213	0.0000	-0.0018	-0.0007	-0.0106
60.0	0.0	0.0	0.0000	0.0000	0.3392	0.0445	0.0237	0.0000	-0.0018	0.0008	-0.0103
60.0	0.0	0.0	0.0000	0.0000	0.3476	0.0459	0.0261	0.0000	-0.0016	0.0023	-0.0092
60.0	0.0	0.0	0.0000	0.0000	0.3560	0.0473	0.0285	0.0000	-0.0012	0.0035	-0.0068
60.0	0.0	0.0	0.0000	0.0000	0.3644	0.0487	0.0309	0.0000	-0.0006	0.0042	-0.0036
60.0	0.0	0.0	0.0000	0.0000	0.3728	0.0501	0.0333	0.0000	-0.0000	0.0045	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.3812	0.0515	0.0357	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.3896	0.0529	0.0381	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.3980	0.0543	0.0405	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4064	0.0557	0.0429	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4148	0.0571	0.0453	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4232	0.0585	0.0477	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4316	0.0599	0.0501	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4400	0.0613	0.0525	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4484	0.0627	0.0549	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4568	0.0641	0.0573	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4652	0.0655	0.0597	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4736	0.0669	0.0621	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4820	0.0683	0.0645	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4904	0.0697	0.0669	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.4988	0.0711	0.0693	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5072	0.0725	0.0717	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5156	0.0739	0.0741	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5240	0.0753	0.0765	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5324	0.0767	0.0789	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5408	0.0781	0.0813	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5492	0.0795	0.0837	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5576	0.0809	0.0861	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5660	0.0823	0.0885	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5744	0.0837	0.0909	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5828	0.0851	0.0933	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5912	0.0865	0.0957	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.5996	0.0879	0.0981	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6080	0.0893	0.1005	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6164	0.0907	0.1029	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6248	0.0921	0.1053	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6332	0.0935	0.1077	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6416	0.0949	0.1101	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6500	0.0963	0.1125	0.0000	-0.0000	0.0000	0.0000
60.0	0.0	0.0	0.0000	0.0000	0.6584	0.0977	0.1149	0.0000	-0.0000	0.0000	0.0000

Table 4 continued, part 6 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$						
75	0	0	0	0072	0	0	0028	-0	0000	0	1442	-0	0000	-0	0108	-0	0000
75	0	0	0	0070	0	0	0029	-0	0037	0	1411	-0	0007	-0	0101	-0	0176
75	0	0	0	0067	0	0	0033	-0	0069	0	1322	-0	0014	-0	0082	-0	0330
75	0	0	0	0061	0	0	0039	-0	0093	0	1186	-0	0019	-0	0034	-0	0449
75	0	0	0	0054	0	0	0046	-0	0106	0	1018	-0	0022	-0	0019	-0	0506
75	0	0	0	0046	0	0	0054	-0	0106	0	0840	-0	0022	-0	0019	-0	0506
75	0	0	0	0039	0	0	0061	-0	0069	0	0672	-0	0019	-0	0034	-0	0449
75	0	0	0	0033	0	0	0067	-0	0069	0	0536	-0	0014	-0	0082	-0	0330
75	0	0	0	0029	0	0	0070	-0	0037	0	0447	-0	0007	-0	0101	-0	0176
75	0	0	0	0028	-0	0	0072	-0	0000	0	0416	-0	0000	-0	0108	-0	0000
75	0	0	0	0025	0	0	0072	-0	0000	0	1436	-0	0000	-0	0102	-0	0000
75	0	0	0	0024	0	0	0072	-0	0000	0	1404	-0	0007	-0	0096	-0	0167
75	0	0	0	0023	0	0	0072	-0	0000	0	1315	-0	0013	-0	0078	-0	0314
75	0	0	0	0022	0	0	0072	-0	0000	0	1178	-0	0018	-0	0051	-0	0423
75	0	0	0	0021	0	0	0072	-0	0000	0	1011	-0	0021	-0	0018	-0	0481
75	0	0	0	0020	0	0	0072	-0	0000	0	0832	-0	0020	-0	0018	-0	0481
75	0	0	0	0019	0	0	0072	-0	0000	0	0665	-0	0018	-0	0051	-0	0422
75	0	0	0	0018	0	0	0072	-0	0000	0	0529	-0	0013	-0	0078	-0	0313
75	0	0	0	0017	0	0	0072	-0	0000	0	0440	-0	0007	-0	0096	-0	0167
75	0	0	0	0016	0	0	0072	-0	0000	0	0409	-0	0000	-0	0102	-0	0000
75	0	0	0	0015	0	0	0072	-0	0000	0	1417	-0	0000	-0	0088	-0	0000
75	0	0	0	0014	0	0	0072	-0	0000	0	1336	-0	0004	-0	0083	-0	0144
75	0	0	0	0013	0	0	0072	-0	0000	0	1296	-0	0012	-0	0067	-0	0271
75	0	0	0	0012	0	0	0072	-0	0000	0	1158	-0	0016	-0	0044	-0	0364
75	0	0	0	0011	0	0	0072	-0	0000	0	0990	-0	0018	-0	0015	-0	0413
75	0	0	0	0010	0	0	0072	-0	0000	0	0812	-0	0018	-0	0016	-0	0413
75	0	0	0	0009	0	0	0072	-0	0000	0	0645	-0	0013	-0	0044	-0	0363
75	0	0	0	0008	0	0	0072	-0	0000	0	0510	-0	0011	-0	0067	-0	0268
75	0	0	0	0007	0	0	0072	-0	0000	0	0421	-0	0006	-0	0082	-0	0143
75	0	0	0	0006	0	0	0072	-0	0000	0	0391	-0	0005	-0	0088	-0	0000
75	0	0	0	0005	0	0	0072	-0	0000	0	1393	-0	0000	-0	0068	-0	0000
75	0	0	0	0004	0	0	0072	-0	0000	0	1361	-0	0003	-0	0064	-0	0112
75	0	0	0	0003	0	0	0072	-0	0000	0	1271	-0	0009	-0	0052	-0	0210
75	0	0	0	0002	0	0	0072	-0	0000	0	1132	-0	0012	-0	0034	-0	0283
75	0	0	0	0001	0	0	0072	-0	0000	0	0964	-0	0014	-0	0011	-0	0319
75	0	0	0	0000	0	0	0072	-0	0000	0	0766	-0	0014	-0	0012	-0	0318
75	0	0	0	0000	0	0	0072	-0	0000	0	0620	-0	0012	-0	0034	-0	0278
75	0	0	0	0000	0	0	0072	-0	0000	0	0483	-0	0009	-0	0053	-0	0205
75	0	0	0	0000	0	0	0072	-0	0000	0	0398	-0	0003	-0	0063	-0	0109
75	0	0	0	0000	0	0	0072	-0	0000	0	0366	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072	-0	0000	0	0369	-0	0000	-0	0067	-0	0000
75	0	0	0	0000	0	0	0072										

Table 4 continued, part 7 of 7.

$\theta_1$	$\theta_2$	$\beta_\phi$	$\sigma_1/\lambda^2$	$\sigma_2/\lambda^2$	$\sigma_3/\lambda^2$	$\sigma_4/\lambda^2$	$\sigma_5/\lambda^2$	$\sigma_6/\lambda^2$	$\sigma_7/\lambda^2$	$\sigma_8/\lambda^2$	$\sigma_9/\lambda^2$
90	0	0	0.0000	-0.0000	0.0409	0.0000	0.0000	0.1435	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0440	0.0000	0.0000	0.1404	0.0000	0.0000	-0.0175
90	0	0	0.0000	-0.0000	0.0329	0.0000	0.0000	0.1315	0.0000	0.0000	-0.0330
90	0	0	0.0000	-0.0000	0.0666	0.0000	0.0000	0.1179	0.0000	0.0000	-0.0444
90	0	0	0.0000	-0.0000	0.0833	0.0000	0.0000	0.1011	0.0000	0.0000	-0.0505
90	0	0	0.0000	-0.0000	0.1011	0.0000	0.0000	0.0833	0.0000	-0.0000	-0.0505
90	0	0	0.0000	-0.0000	0.1179	0.0000	0.0000	0.0666	0.0000	-0.0000	-0.0444
90	0	0	0.0000	-0.0000	0.1315	0.0000	0.0000	0.0529	0.0000	-0.0000	-0.0330
90	0	0	0.0000	-0.0000	0.1404	0.0000	0.0000	0.0440	0.0000	-0.0000	-0.0175
90	0	0	0.0000	-0.0000	0.1435	0.0000	-0.0000	0.0409	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0376	0.0000	0.0000	0.1429	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0404	0.0000	0.0000	0.1398	0.0000	0.0000	-0.0167
90	0	0	0.0000	-0.0000	0.0483	0.0000	0.0000	0.1308	0.0000	0.0000	-0.0314
90	0	0	0.0000	-0.0000	0.0609	0.0000	0.0000	0.1171	0.0000	0.0000	-0.0423
90	0	0	0.0000	-0.0000	0.0740	0.0000	0.0000	0.1004	0.0000	0.0000	-0.0481
90	0	0	0.0000	-0.0000	0.0921	0.0000	0.0000	0.0825	0.0000	-0.0000	-0.0480
90	0	0	0.0000	-0.0000	0.1073	0.0000	0.0000	0.0638	0.0000	-0.0000	-0.0422
90	0	0	0.0000	-0.0000	0.1196	0.0000	0.0000	0.0522	0.0000	-0.0000	-0.0313
90	0	0	0.0000	-0.0000	0.1276	0.0000	0.0000	0.0433	0.0000	-0.0000	-0.0167
90	0	0	0.0000	-0.0000	0.1304	0.0000	-0.0000	0.0403	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0291	0.0000	0.0000	0.1410	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0311	0.0000	0.0000	0.1379	0.0000	0.0000	-0.0144
90	0	0	0.0000	-0.0000	0.0372	0.0000	0.0000	0.1289	0.0000	0.0000	-0.0271
90	0	0	0.0000	-0.0000	0.0463	0.0000	0.0000	0.1152	0.0000	0.0000	-0.0364
90	0	0	0.0000	-0.0000	0.0575	0.0000	0.0000	0.0984	0.0000	0.0000	-0.0413
90	0	0	0.0000	-0.0000	0.0694	0.0000	0.0000	0.0806	0.0000	-0.0000	-0.0413
90	0	0	0.0000	-0.0000	0.0803	0.0000	0.0000	0.0639	0.0000	-0.0000	-0.0362
90	0	0	0.0000	-0.0000	0.0895	0.0000	0.0000	0.0503	0.0000	-0.0000	-0.0268
90	0	0	0.0000	-0.0000	0.0954	0.0000	0.0000	0.0413	0.0000	-0.0000	-0.0143
90	0	0	0.0000	-0.0000	0.0974	0.0000	-0.0000	0.0383	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0183	0.0000	0.0000	0.1386	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0156	0.0000	0.0000	0.1355	0.0000	0.0000	-0.0112
90	0	0	0.0000	-0.0000	0.0232	0.0000	0.0000	0.1264	0.0000	0.0000	-0.0210
90	0	0	0.0000	-0.0000	0.0287	0.0000	0.0000	0.1126	0.0000	0.0000	-0.0281
90	0	0	0.0000	-0.0000	0.0333	0.0000	0.0000	0.0937	0.0000	0.0000	-0.0319
90	0	0	0.0000	-0.0000	0.0423	0.0000	0.0000	0.0779	0.0000	-0.0000	-0.0317
90	0	0	0.0000	-0.0000	0.0488	0.0000	0.0000	0.0613	0.0000	-0.0000	-0.0278
90	0	0	0.0000	-0.0000	0.0541	0.0000	0.0000	0.0479	0.0000	-0.0000	-0.0206
90	0	0	0.0000	-0.0000	0.0576	0.0000	0.0000	0.0392	0.0000	-0.0000	-0.0109
90	0	0	0.0000	-0.0000	0.0587	0.0000	-0.0000	0.0362	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0087	0.0000	0.0000	0.1363	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0093	0.0000	0.0000	0.1331	0.0000	0.0000	-0.0075
90	0	0	0.0000	-0.0000	0.0109	0.0000	0.0000	0.1240	0.0000	0.0000	-0.0141
90	0	0	0.0000	-0.0000	0.0133	0.0000	0.0000	0.1101	0.0000	0.0000	-0.0188
90	0	0	0.0000	-0.0000	0.0162	0.0000	0.0000	0.0932	0.0000	0.0000	-0.0213
90	0	0	0.0000	-0.0000	0.0193	0.0000	0.0000	0.0754	0.0000	-0.0000	-0.0212
90	0	0	0.0000	-0.0000	0.0222	0.0000	0.0000	0.0589	0.0000	-0.0000	-0.0185
90	0	0	0.0000	-0.0000	0.0245	0.0000	0.0000	0.0456	0.0000	-0.0000	-0.0137
90	0	0	0.0000	-0.0000	0.0260	0.0000	0.0000	0.0370	0.0000	-0.0000	-0.0072
90	0	0	0.0000	-0.0000	0.0265	0.0000	-0.0000	0.0340	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0022	0.0000	0.0000	0.1347	-0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0024	0.0000	0.0000	0.1315	0.0000	0.0000	-0.0037
90	0	0	0.0000	-0.0000	0.0028	0.0000	0.0000	0.1223	0.0000	0.0000	-0.0070
90	0	0	0.0000	-0.0000	0.0034	0.0000	0.0000	0.1083	0.0000	0.0000	-0.0094
90	0	0	0.0000	-0.0000	0.0041	0.0000	0.0000	0.0914	0.0000	0.0000	-0.0106
90	0	0	0.0000	-0.0000	0.0049	0.0000	0.0000	0.0737	0.0000	-0.0000	-0.0103
90	0	0	0.0000	-0.0000	0.0056	0.0000	0.0000	0.0573	0.0000	-0.0000	-0.0092
90	0	0	0.0000	-0.0000	0.0061	0.0000	0.0000	0.0440	0.0000	-0.0000	-0.0068
90	0	0	0.0000	-0.0000	0.0065	0.0000	0.0000	0.0335	0.0000	-0.0000	-0.0036
90	0	0	0.0000	-0.0000	0.0066	0.0000	-0.0000	0.0329	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1341	-0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1309	0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1217	0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.1077	0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0908	0.0000	-0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0731	0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0567	0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0435	0.0000	0.0000	0.0000
90	0	0	0.0000	-0.0000	0.0000	0.0000	0.0000	0.0350	0.0000	0.0000	0.0000
90	0	0	0.0000	0.0000	0.0000	0.0000	-0.0000	0.0320	0.0000	0.0000	-0.0000

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